

## Hydraulic Conductivity Testing

Hydraulic conductivity (slug) tests were performed on each of the four new monitoring wells installed at the site for the feasibility study, including water table wells MW-29, MW-30, and MW-31 and piezometer MW-30P. The slug tests were performed by rapidly lowering a solid cylinder (slug) into the well to cause an instantaneous rise in water level (falling head test), then measuring the return of the water level to its static condition. A second test was performed by removing the slug (rising head test), and again measuring the response of the water level in the well. Water level data were recorded with an In-Situ, Inc. automated pressure transducer (Level TROLL 700) and data logger system. Slug test data were evaluated using Waterloo Hydrologic Aquifer Test Pro v. 2013.1 graphical analysis and reporting software. The slug tests were analyzed using the methods of Bouwer and Rice (1976)<sup>1</sup> for unconfined aquifers.

Hydraulic conductivity values (recovery test only) calculated for water table observation wells ranged from  $1.1 \times 10^{-2}$  cm/sec in well MW-29, screened primarily in silty sand, silt and clay deposits, to  $1.4 \times 10^{-3}$  cm/sec in well MW-31, screened in silty sand and clay deposits. The hydraulic conductivity value calculated for the piezometer, which is screened in silty sand, was  $2.1 \times 10^{-2}$  cm/sec.

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<sup>1</sup> Bouwer, H. and R.C. Rice, A Slug Test for Determining Hydraulic Conductivity of Unconfined Aquifers with Completely or Partially Penetrating Wells, *Water Resources Research*, Vol.12, No.3, 1976, pp.423-428

Table \_  
Summary of Slug Test Parameters  
Adams County Landfill

Well Number	Test Number	Depth of Well (ft)	Depth to Water (ft)	Initial Drawdown Elevation (t <sub>0</sub> ) (ft)	Internal Well Radius (r) (ft)	Effective Well Radius (R) (ft)	Sat. Aquifer Thickness (ft)	Screen Length (L) (ft)	Height of Water Column (b) (ft)
MW-29	Slug In	34.1	24.76	24.95	0.083	0.33	9.34	10	9.34
	Slug Out			22.76					
MW-30	Slug In	46.9	38.48	39.03	0.083	0.33	8.42	9	8.42
	Slug Out			37.77					
MW-30P	Slug In	75.8	44.22	46.4	0.083	0.33	32	5	31.58
	Slug Out			42.36					
MW-31	Slug In	41.4	32.70	33.15	0.083	0.33	8.70	9	8.70
	Slug Out			30.59					



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### Slug Test Analysis Report

Project: Adams County Landfill

Number: 10-1070.12

Client: Adams County Solid Waste Department

Location: Adams, WI

Slug Test: MW-29 Slug Out

Test Well: MW-29

Test Conducted by: Jeff Steiner

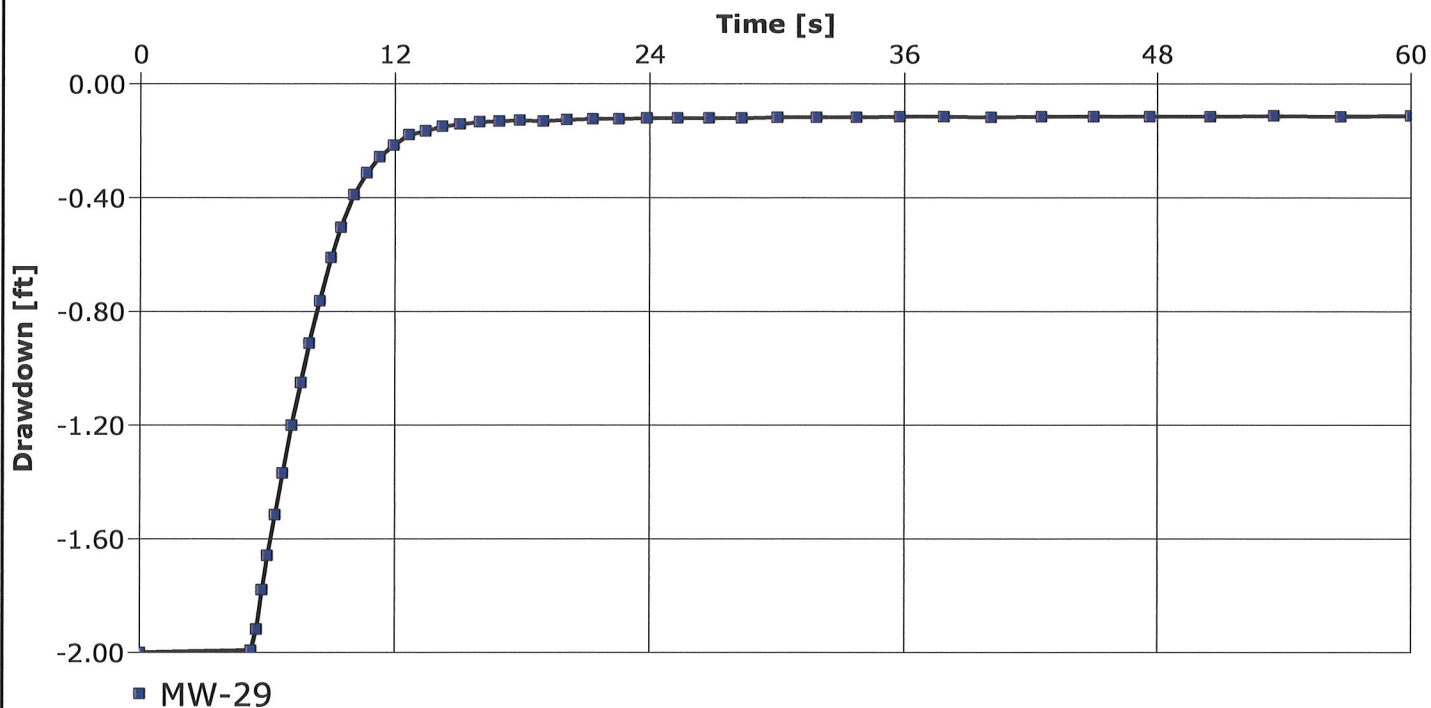
Test Date: 1/28/2016

Analysis Performed by: Jeff Steiner

MW-29 Slug Out Time-Drawdown

Analysis Date: 1/29/2016

Aquifer Thickness: 10.00 ft





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## Slug Test Analysis Report

Project: Adams County Landfill

Number: 10-1070.12

Client: Adams County Solid Waste Department

Location: Adams, WI

Slug Test: MW-29 Slug Out

Test Well: MW-29

Test Conducted by: Jeff Steiner

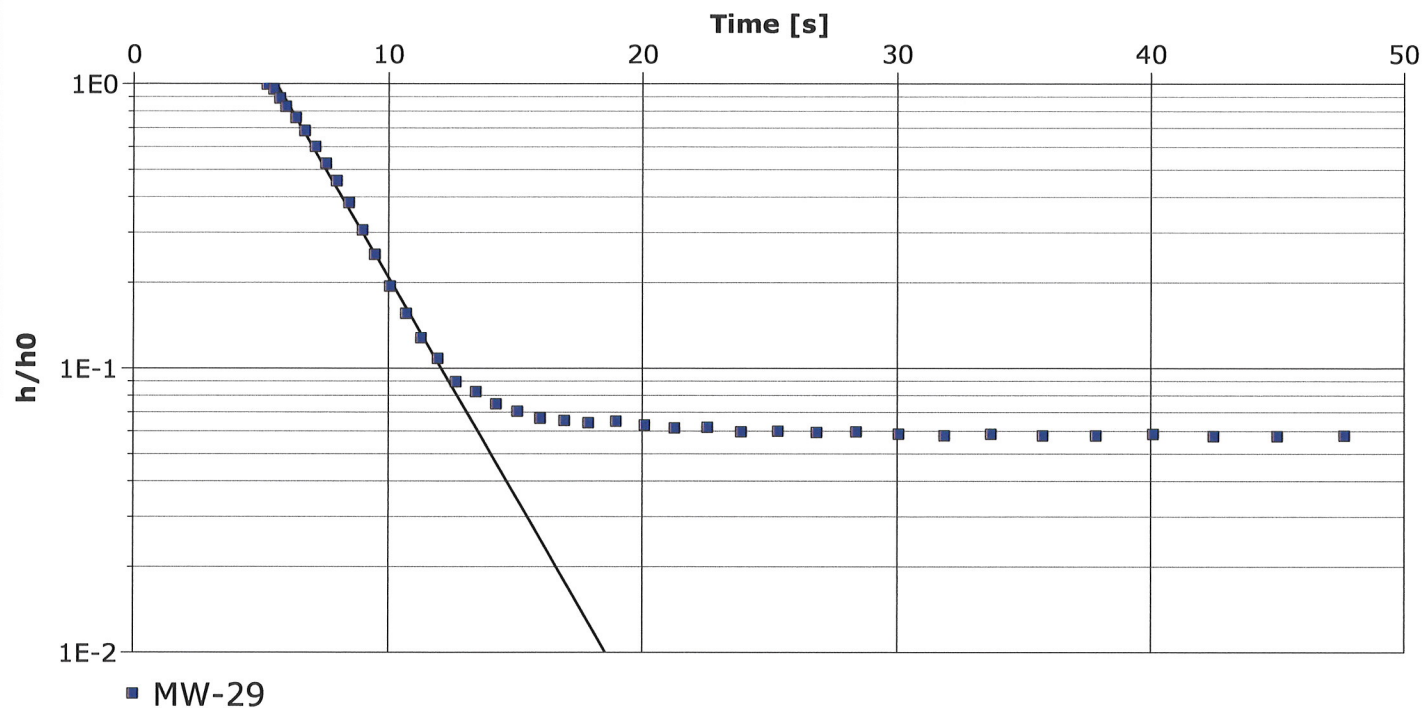
Test Date: 1/28/2016

Analysis Performed by: Jeff Steiner

MW-29 Slug Out Bouwer & Rice

Analysis Date: 1/29/2016

Aquifer Thickness: 10.00 ft



Calculation using Bouwer & Rice

Observation Well

Hydraulic Conductivity  
[ft/s]

MW-29

$3.80 \times 10^{-4}$





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### Slug Test Analysis Report

Project: Adams County Landfill

Number: 10-1070.12

Client: Adams County Solid Waste Department

Location: Adams, WI

Slug Test: MW-30 Slug In

Test Well: MW-30

Test Conducted by: Jeff Steiner

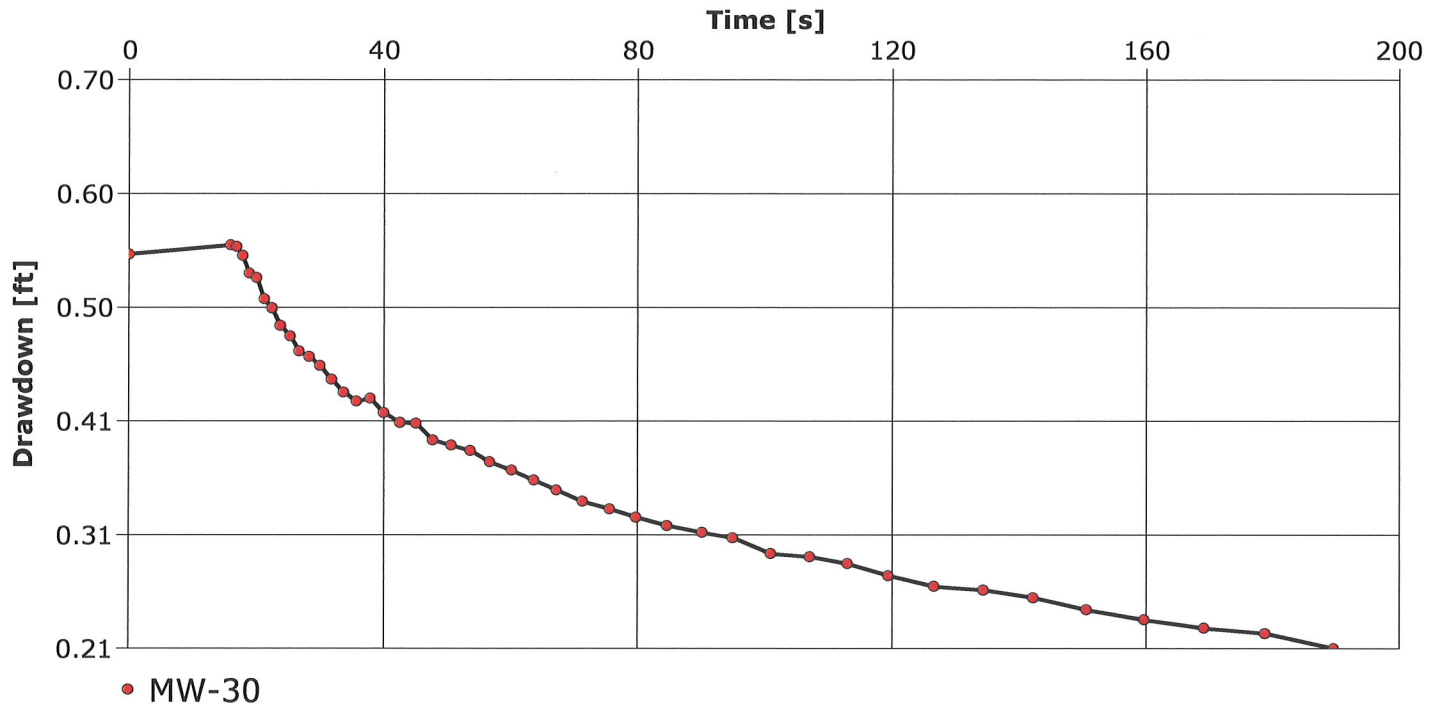
Test Date: 1/28/2016

Analysis Performed by: Jeff Steiner

MW-30 Slug In Time-Drawdown

Analysis Date: 1/29/2016

Aquifer Thickness: 8.42 ft





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### Slug Test Analysis Report

Project: Adams County Landfill

Number: 10-1070.12

Client: Adams County Solid Waste Department

Location: Adams, WI

Slug Test: MW-30 Slug In

Test Well: MW-30

Test Conducted by: Jeff Steiner

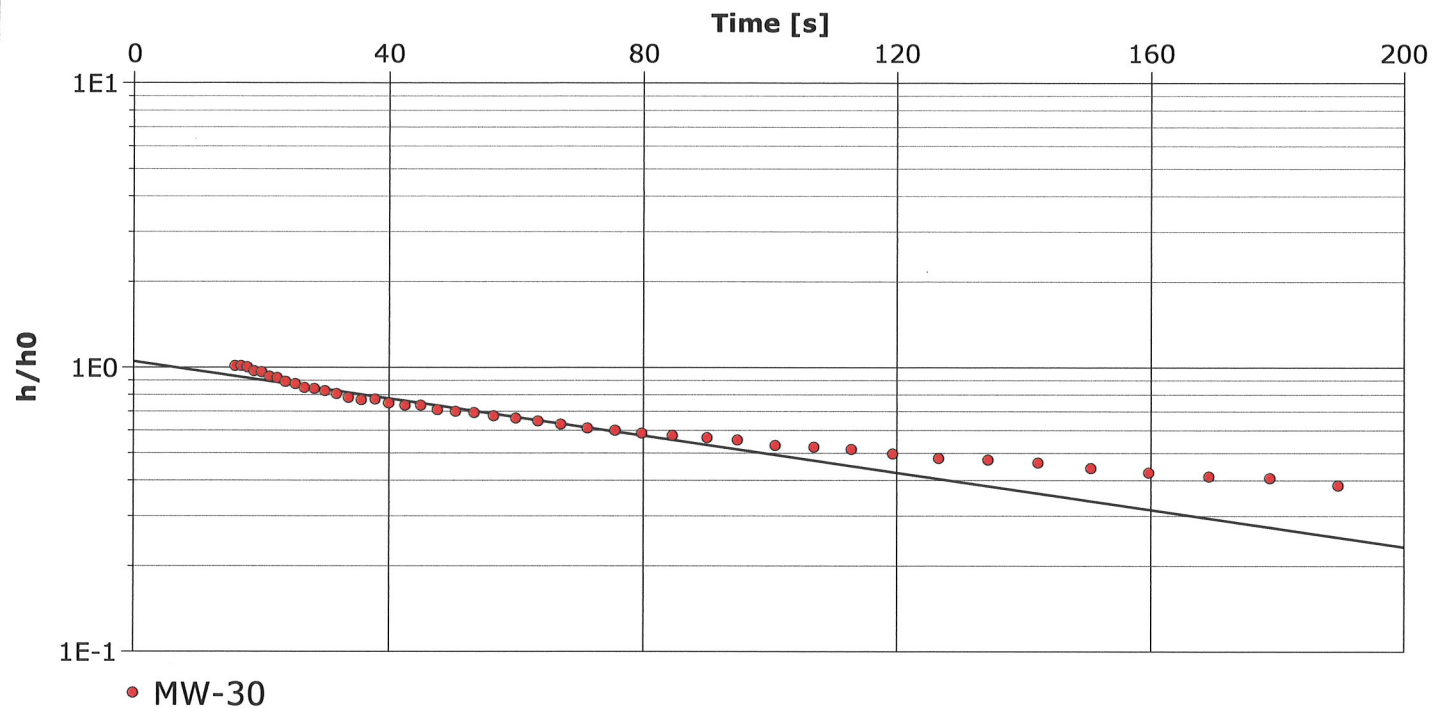
Test Date: 1/28/2016

Analysis Performed by: Jeff Steiner

MW-30 Slug In Bouwer & Rice

Analysis Date: 1/29/2016

Aquifer Thickness: 8.42 ft



Calculation using Bouwer & Rice

Observation Well

Hydraulic Conductivity  
[ft/s]

MW-30

$8.68 \times 10^{-6}$



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## Slug Test Analysis Report

Project: Adams County Landfill

Number: 10-1070.12

Client: Adams County Solid Waste Department

Location: Adams, WI

Slug Test: MW-30 Slug Out

Test Well: MW-30

Test Conducted by: Jeff Steiner

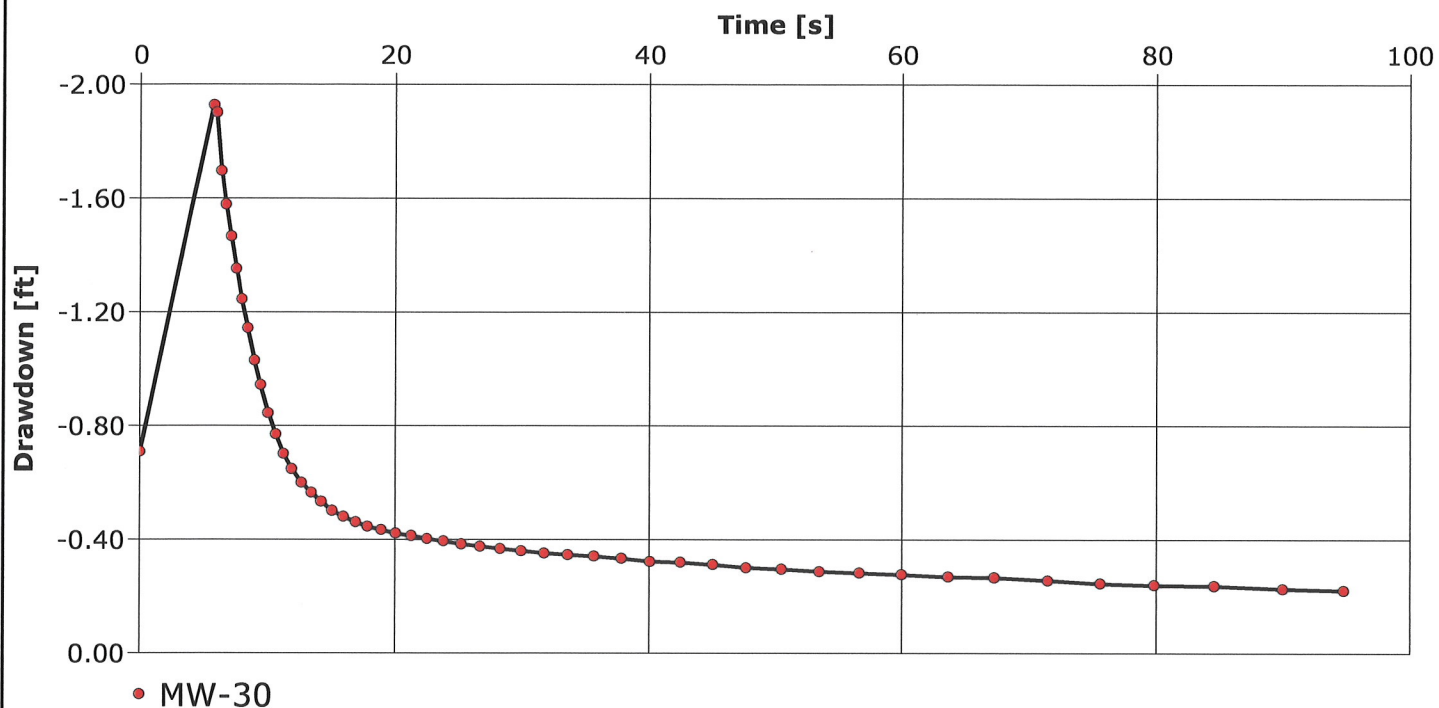
Test Date: 1/28/2016

Analysis Performed by: Jeff Steiner

MW-30 Slug Out Time-Drawdown

Analysis Date: 1/29/2016

Aquifer Thickness: 8.42 ft





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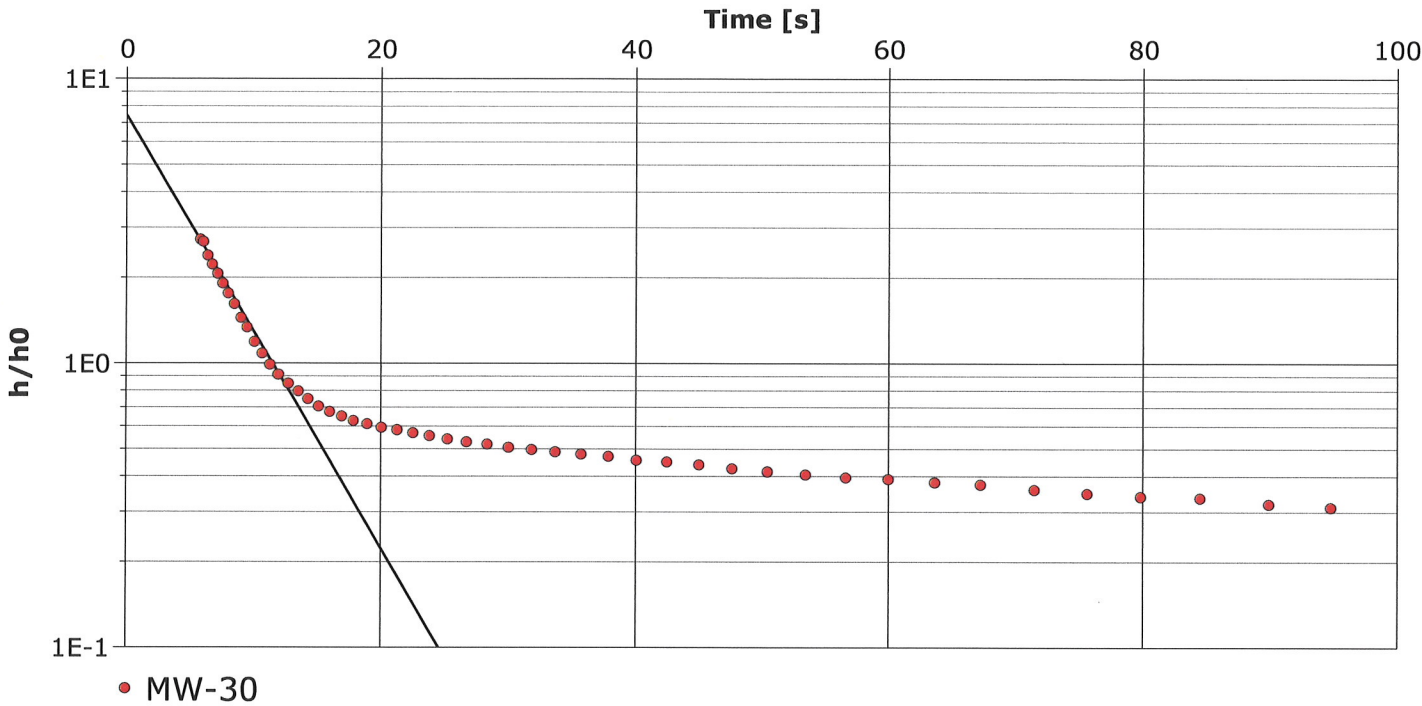
Slug Test Analysis Report

Project: Adams County Landfill

Number: 10-1070.12

Client: Adams County Solid Waste Department

Location: Adams, WI	Slug Test: MW-30 Slug Out	Test Well: MW-30
Test Conducted by: Jeff Steiner		Test Date: 1/28/2016
Analysis Performed by: Jeff Steiner	MW-30 Slug Out Bouwer & Rice	Analysis Date: 1/29/2016
Aquifer Thickness: 8.42 ft		



Calculation using Bouwer & Rice		
Observation Well	Hydraulic Conductivity [ft/s]	
MW-30	$2.02 \times 10^{-4}$	



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### Slug Test Analysis Report

Project: Adams County Landfill

Number: 10-1070.12

Client: Adams County Solid Waste Department

Location: Adams, WI

Slug Test: MW-30P Slug In

Test Well: MW-30P

Test Conducted by: Jeff Steiner

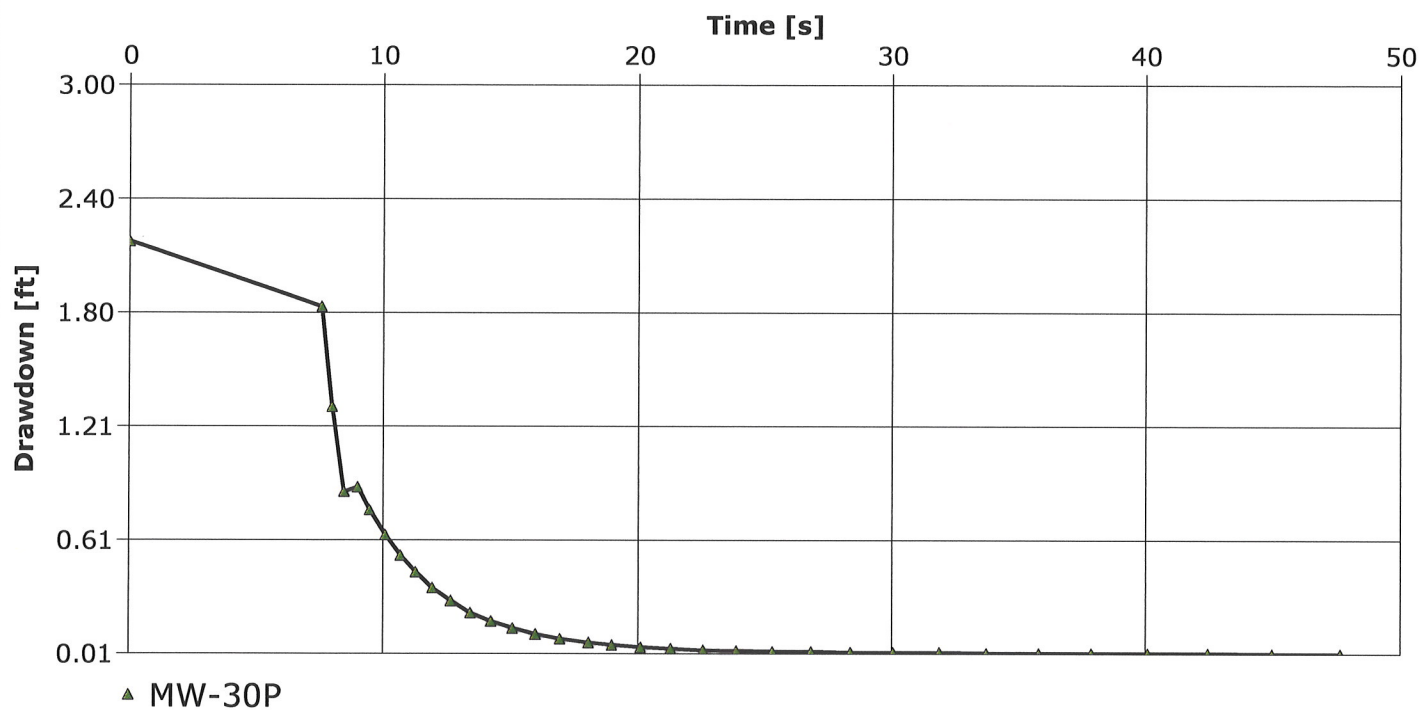
Test Date: 1/28/2016

Analysis Performed by: Jeff Steiner

MW-30P Slug In Time-Drawdown

Analysis Date: 1/29/2016

Aquifer Thickness: 32.00 ft







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Slug Test Analysis Report

Project: Adams County Landfill

Number: 10-1070.12

Client: Adams County Solid Waste Department

Location: Adams, WI

Slug Test: MW-30P Slug In

Test Well: MW-30P

Test Conducted by: Jeff Steiner

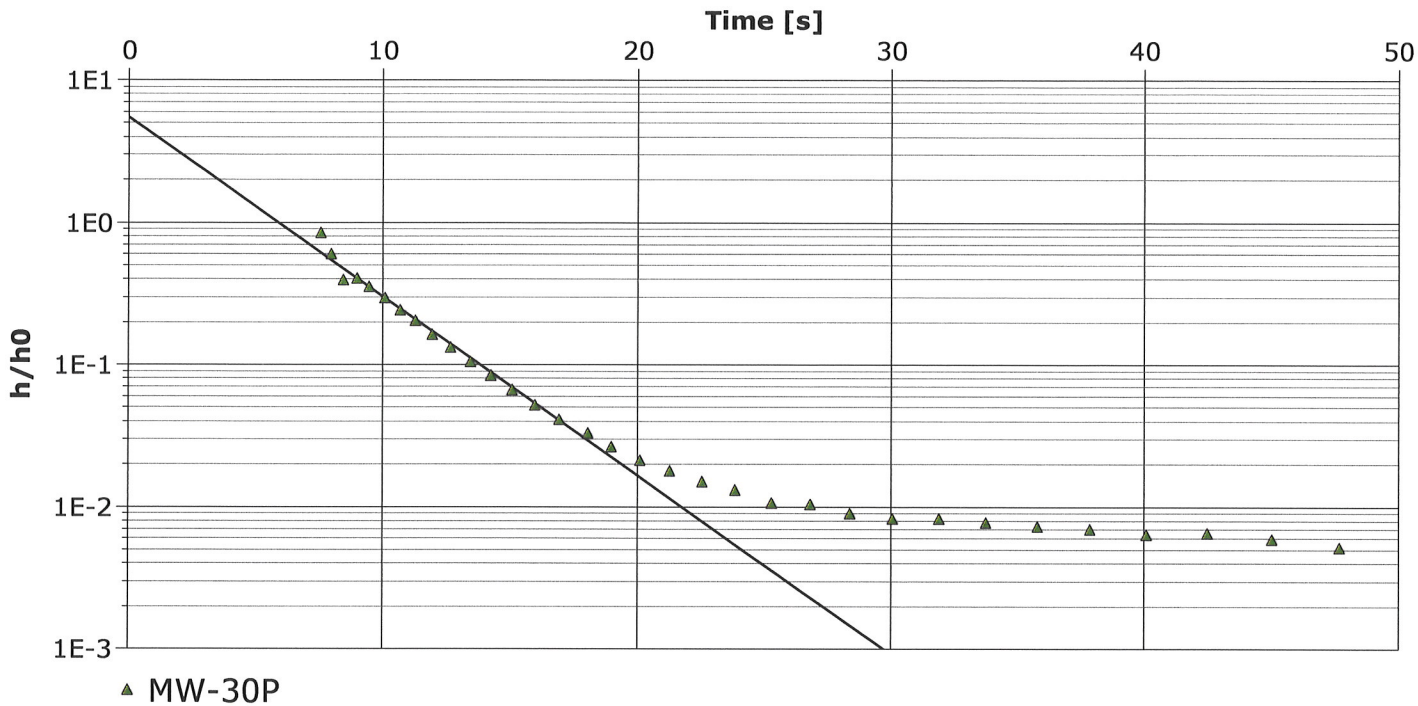
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Analysis Performed by: Jeff Steiner

MW-30 Slug In Bouwer & Rice

Analysis Date: 1/29/2016

Aquifer Thickness: 32.00 ft



Calculation using Bouwer & Rice

Observation Well

Hydraulic Conductivity  
[ft/s]

MW-30P

$6.31 \times 10^{-4}$



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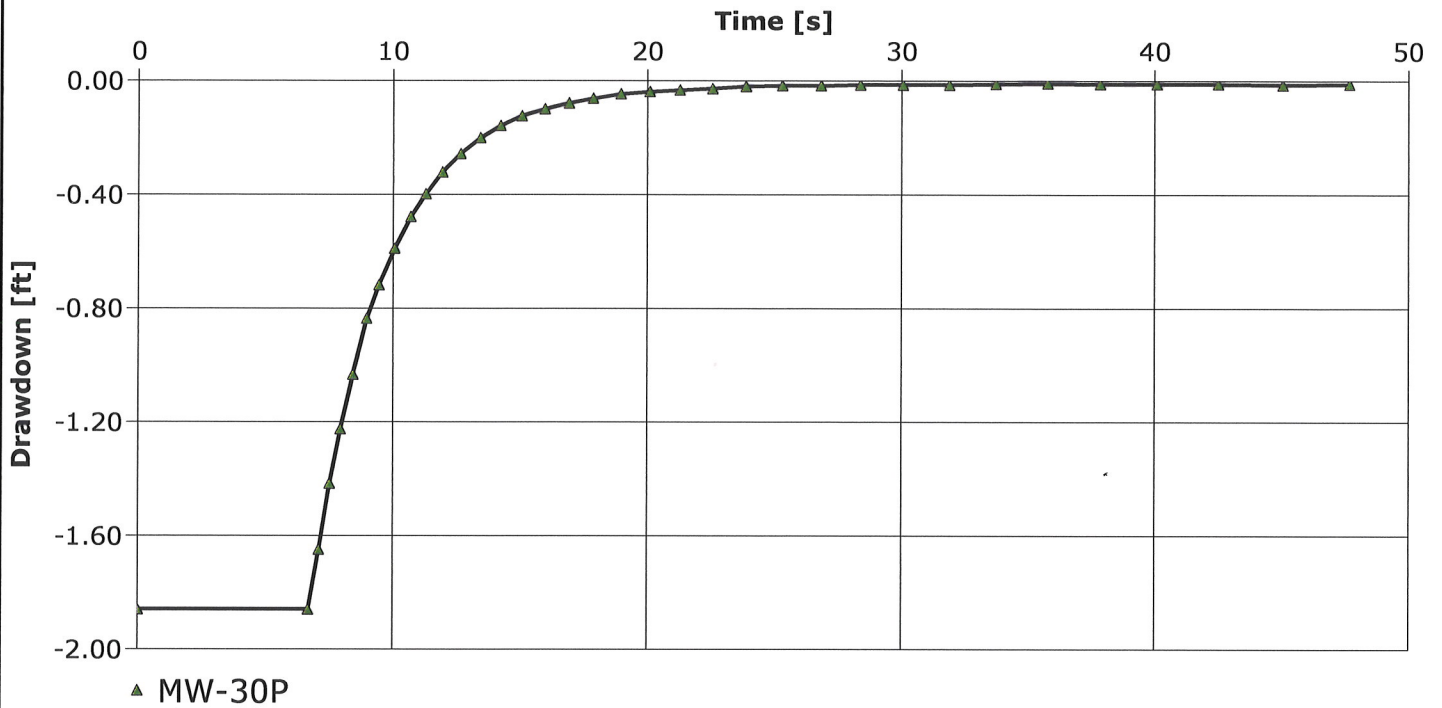
### Slug Test Analysis Report

Project: Adams County Landfill

Number: 10-1070.12

Client: Adams County Solid Waste Department

Location: Adams, WI	Slug Test: MW-30P Slug Out	Test Well: MW-30P
Test Conducted by: Jeff Steiner		Test Date: 1/28/2016
Analysis Performed by: Jeff Steiner	MW-30P Slug Out	Analysis Date: 1/29/2016
Aquifer Thickness: 32.00 ft		







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### Slug Test Analysis Report

Project: Adams County Landfill

Number: 10-1070.12

Client: Adams County Solid Waste Department

Location: Adams, WI

Slug Test: MW-30P Slug Out

Test Well: MW-30P

Test Conducted by: Jeff Steiner

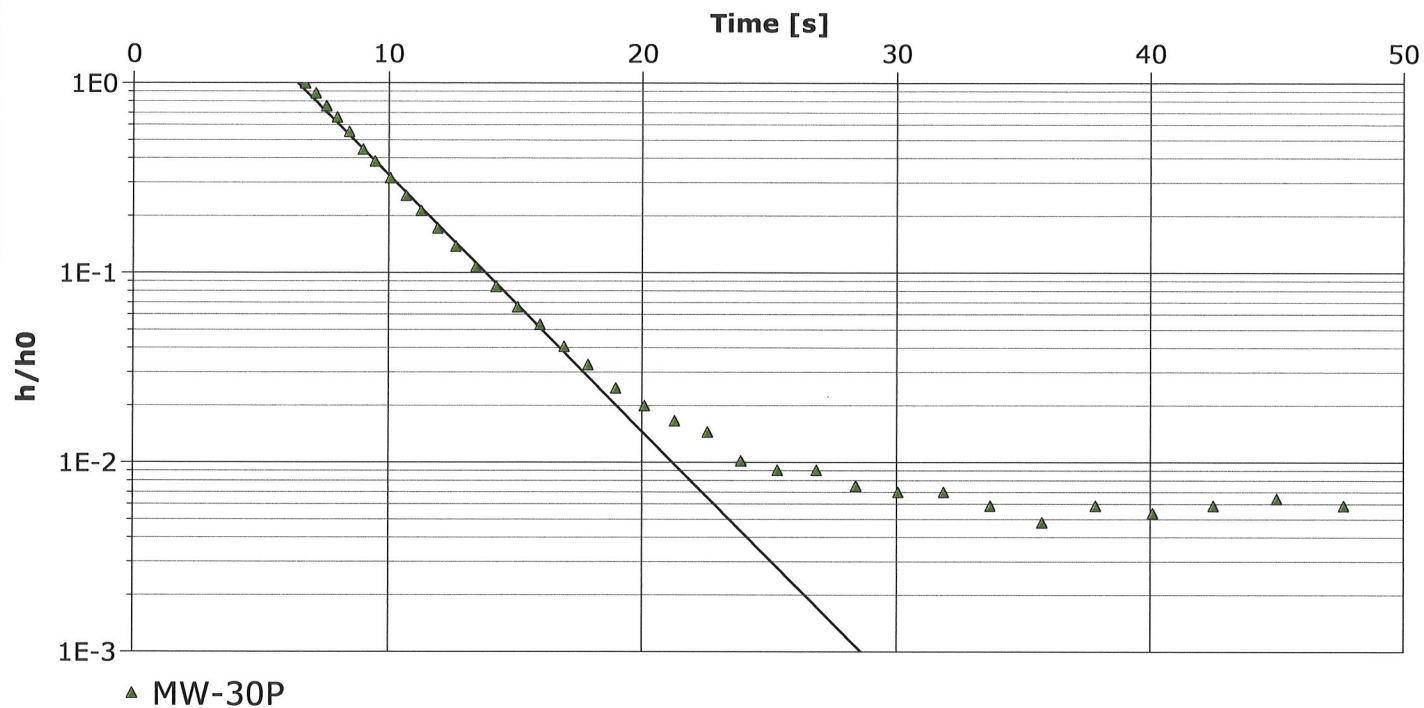
Test Date: 1/28/2016

Analysis Performed by: Jeff Steiner

MW-30P Slug Out Bouwer & Rice

Analysis Date: 1/29/2016

Aquifer Thickness: 32.00 ft



Calculation using Bouwer & Rice

Observation Well

Hydraulic Conductivity  
[ft/s]

MW-30P

$6.79 \times 10^{-4}$



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### Slug Test Analysis Report

Project: Adams County Landfill

Number: 10-1070.12

Client: Adams County Solid Waste Department

Location: Adams, WI

Slug Test: MW-31 Slug In

Test Well: MW-31

Test Conducted by: Jeff Steiner

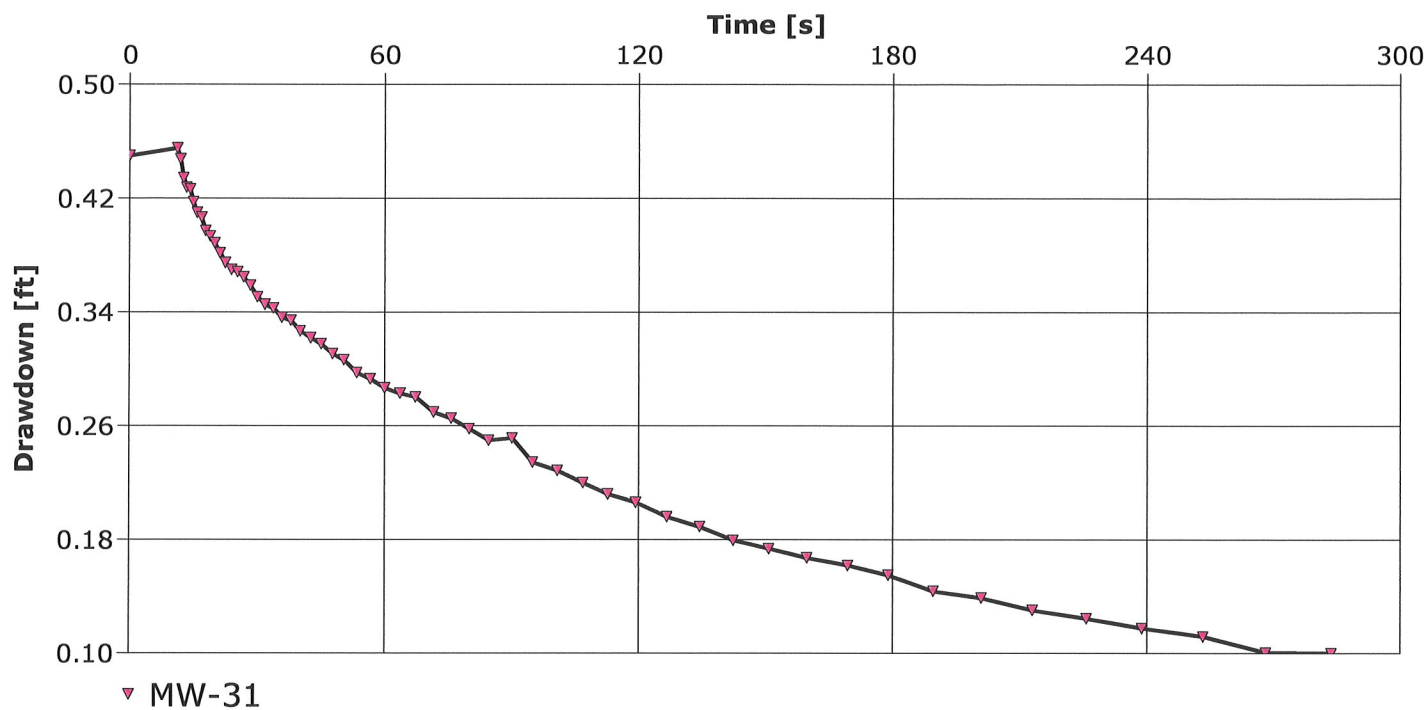
Test Date: 1/28/2016

Analysis Performed by:

MW-31 Slug In Time-Drawdown

Analysis Date: 1/29/2016

Aquifer Thickness: 8.70 ft





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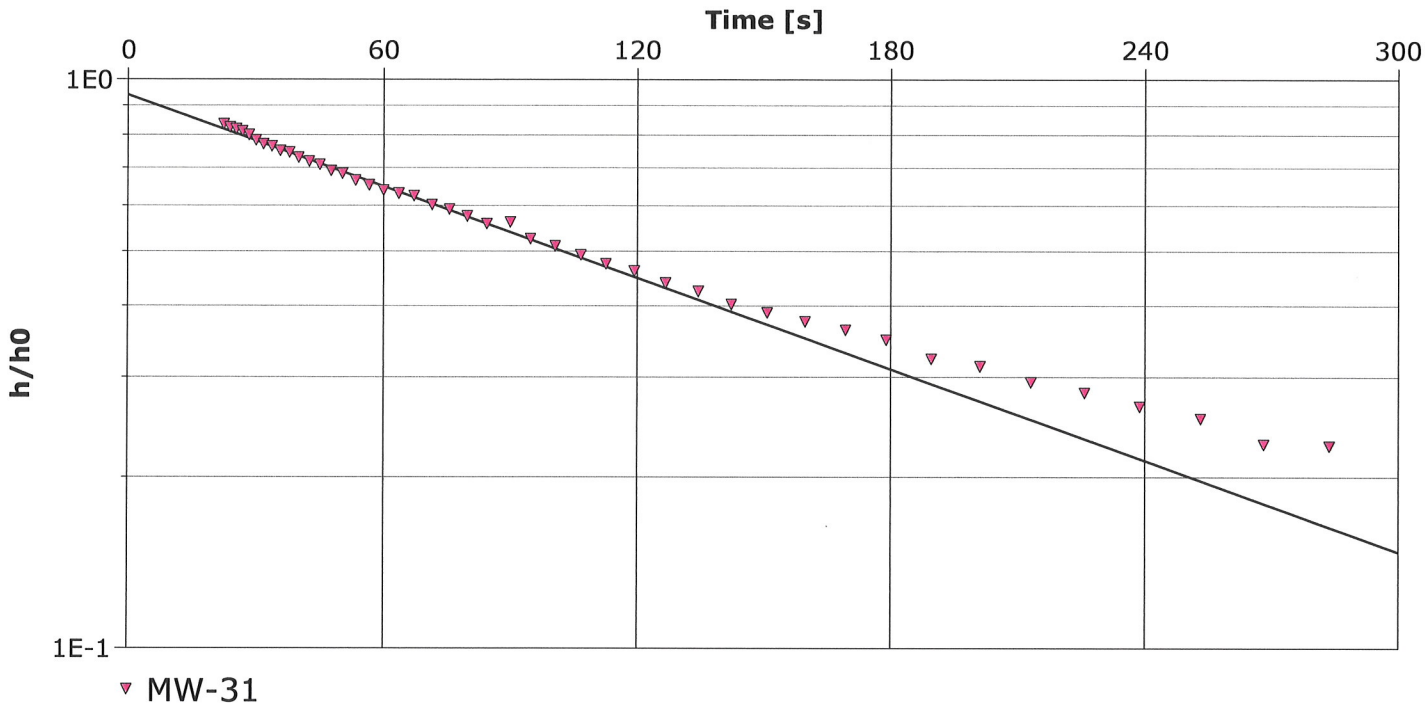
**Slug Test Analysis Report**

Project: Adams County Landfill

Number: 10-1070.12

Client: Adams County Solid Waste Department

Location: Adams, WI	Slug Test: MW-31 Slug In	Test Well: MW-31
Test Conducted by: Jeff Steiner		Test Date: 1/28/2016
Analysis Performed by: Jeff Steiner	MW-31 Slug In Bouwer & Rice	Analysis Date: 1/29/2016
Aquifer Thickness: 8.70 ft		



Calculation using Bouwer & Rice		
Observation Well	Hydraulic Conductivity [ft/s]	
MW-31	$7.11 \times 10^{-6}$	



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### Slug Test Analysis Report

Project: Adams County Landfill

Number: 10-1070.12

Client: Adams County Solid Waste Department

Location: Adams, WI

Slug Test: MW-31 Slug Out

Test Well: MW-31

Test Conducted by: Jeff Steiner

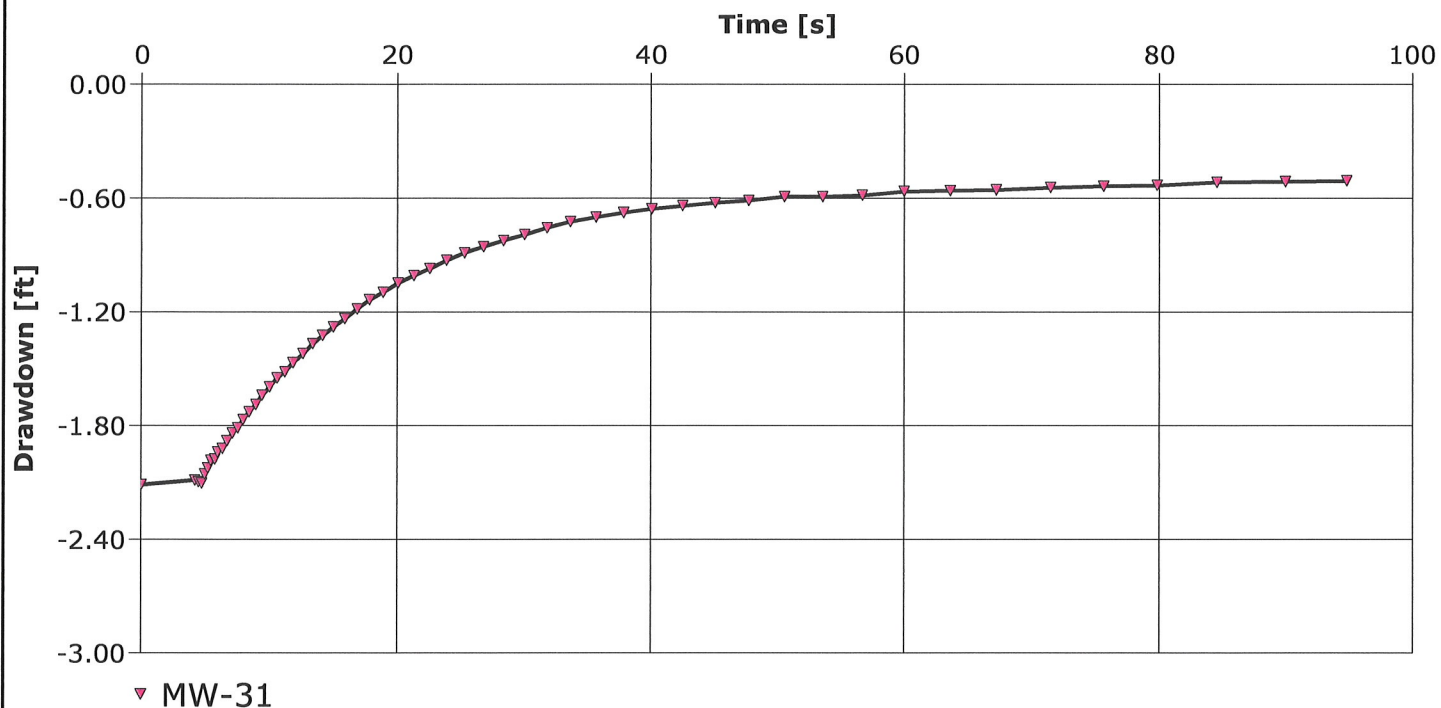
Test Date: 1/28/2016

Analysis Performed by: Jeff Steiner

MW-31 Slug Out Time-Drawdown

Analysis Date: 1/29/2016

Aquifer Thickness: 8.70 ft





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### Slug Test Analysis Report

Project: Adams County Landfill

Number: 10-1070.12

Client: Adams County Solid Waste Department

Location: Adams, WI

Slug Test: MW-31 Slug Out

Test Well: MW-31

Test Conducted by: Jeff Steiner

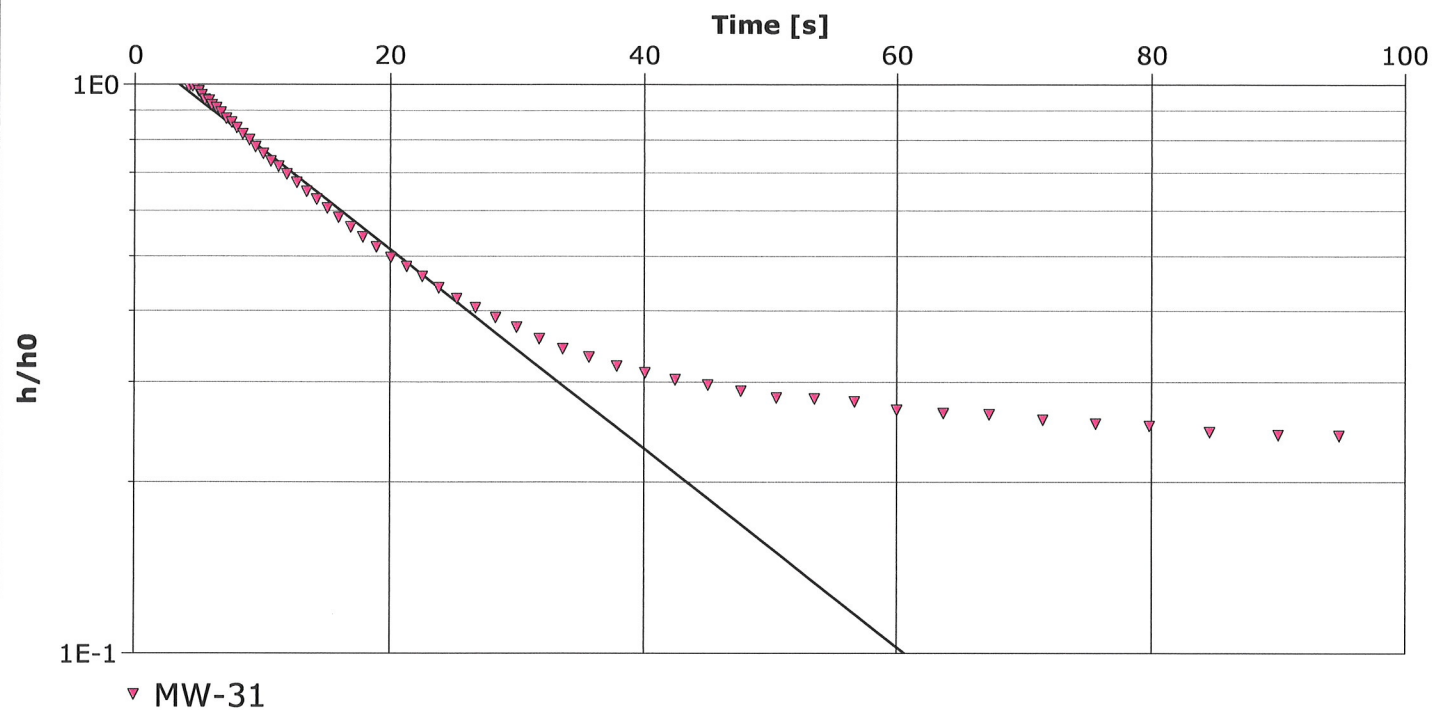
Test Date: 1/28/2016

Analysis Performed by: Jeff Steiner

MW-31 Slug Out Bouwer & Rice

Analysis Date: 1/29/2016

Aquifer Thickness: 8.70 ft



Calculation using Bouwer & Rice

Observation Well

Hydraulic Conductivity  
[ft/s]

MW-31

$4.65 \times 10^{-5}$

## INFIELD PERMEABILITY REPORT

### Bail Down Test Methodology

Each bail down test was conducted by initially putting a pressure transducer, with LCD readout in feet, into a well below the static water level. After recording the initial water level, a four foot by 3/4-inch galvanized iron pipe was lowered below the water level, the water was allowed to stabilize and the stabilized reading was recorded. The pipe was then removed from the well. At the instant the minimum water level reading was recorded (a few seconds into the test) a stopwatch was started and rising water level measurements (h) with time (t) were recorded.

The analytical methodology used to evaluate these data is based upon theory presented by Spangler and Handy\*.

The formula for hydraulic conductivity is:

$$K = 0.617 * \frac{r}{S*d} * \frac{dh}{dt} * 30.48 \text{ cm/ft}$$

Where:

K = hydraulic conductivity (cm/second)

r = borehole radius (ft)

S = a coefficient which is dependent on the ratios h/d and r/d (Fig. 11-11 of Soil Engineering),

$d$  = depth of borehole below water table (ft).

$h$  = depth (ft) of water in hole at the time  $dh/dt$  is determined

$dh/dt$  = rate of rise of water level (ft/second) in hole at depth  $h$ , and

$t$  = time (seconds),

- \* Spangler, M.G. and R.L. Handy, Soil Engineering, 3rd Edition, Intext Educational Publishers, New York, 1973, p. 253-256.



## Slug Test Methodology

Each slug test was conducted by initially putting a pressure transducer, with LCD readout in feet, into a well below the static water level. After recording the initial starting level (H), a four foot by 3/4-inch galvanized iron pipe (slug) was lowered below the water level and the maximum water level reading (H<sub>o</sub>) recorded. At the instant this maximum water level was reached (a few seconds into the test), a stopwatch was started and declining water level measurements (h) with time (t) were recorded.

Also noted for the purposes of data evaluation were the well casing diameter (r), the boring diameter (R), and the well screen length (L).

The analytical methodology used to evaluate these data is based upon theory presented by Freeze and Cherry\*. The formula for hydraulic conductivity (K) is:

$$K = \frac{r^2 \ln(L/R)}{2 L T_o}$$

The key variable in this equation is T<sub>o</sub>, the basic time lag. T<sub>o</sub> is derived by plotting the natural logarithm of the residual head ratio (RHR - the ratio of [h-H], the difference between the maximum rise in water level and the starting water level), against the time (t) at which the head measurement (h) was taken. On semi-log paper these points plot as a straight line.

FIGURE NO. H-1

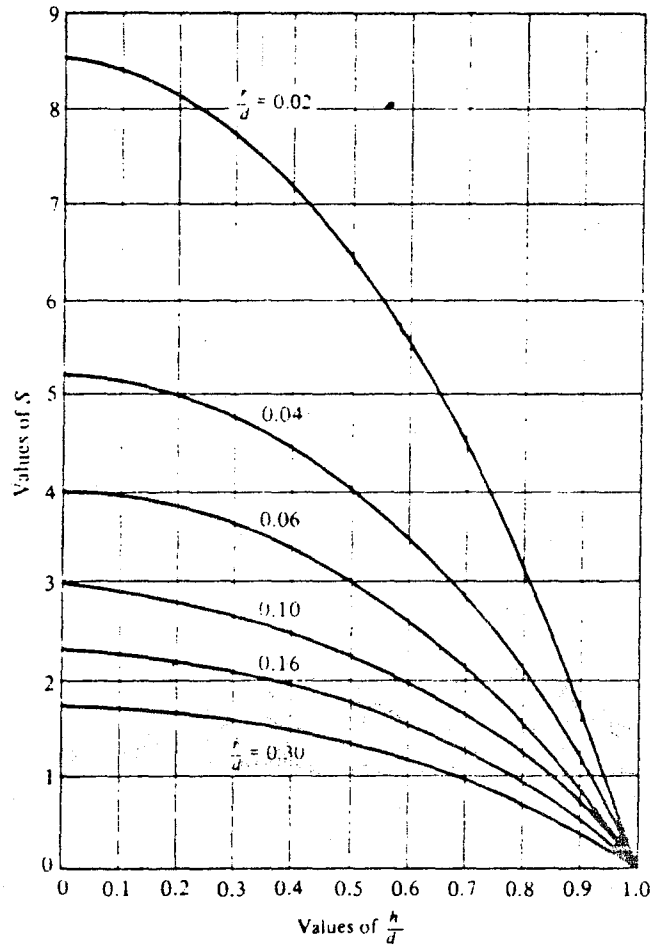


Fig. 11-11. Values of  $S$  in Eq. (11-17).

Source: Spangler, M.G. and R.L. Handy, Soil Engineering, 3rd. Edition, Intext Educational Publishers, New York, 1973, p. 255

WATER TABLE MONITORING WELL  
HYDRAULIC CONDUCTIVITY SUMMARY

Well	t (sec)	r (ft)	d (ft)	r/d	h (ft)	h/d	S	dh/dt (ft/s)	K (cm/s)
MW-1*	10	0.292	11.95	0.02	11.89	0.99	0.1	0.015	$6.9 \times 10^{-2}$
MW-2*	40	0.292	12.56	0.02	11.90	0.95	0.8	0.002	$1.1 \times 10^{-3}$
MW-3*	15	0.292	13.32	0.02	12.62	0.95	0.8	0.015	$7.7 \times 10^{-3}$
MW-6	15	0.333	11.60	0.03	10.90	0.94	0.8	0.007	$4.7 \times 10^{-3}$
MW-7	5	0.333	5.62	0.06	5.24	0.93	0.6	0.022	$4.1 \times 10^{-2}$
MW-8	15	0.333	7.21	0.05	6.71	0.93	0.7	0.007	$8.7 \times 10^{-3}$
MW-9	10	0.333	3.53	0.09	3.02	0.86	1.0	0.0075	$1.3 \times 10^{-2}$
MW-16	15	0.333	6.70	0.05	6.18	0.92	0.8	0.014	$1.6 \times 10^{-2}$
MW-17	15	0.333	10.58	0.03	9.84	0.93	1.1	0.010	$5.4 \times 10^{-3}$
MW-18	15	0.333	6.40	0.05	5.91	0.92	0.8	0.013	$1.6 \times 10^{-2}$

\*Screen wrapped in filter fabric

The slope of this line is used to determine the time (t) at which  $\ln(RHR)$  is -1. This time value is  $T_0$ , which is then used in the above equation to calculate the value of hydraulic conductivity for the test.

\* Freeze, R.A. and J.A. Cherry, Groundwater,  
Prentice-Hall, Inc. Englewood Cliffs, New Jersey,  
1979, pp. 340-341.

IN FIELD HYDRAULIC CONDUCTIVITY SUMMARY  
PIEZOMETER RESULTS - SLUG TEST METHOD

<u>Well</u>	<u>K (cm/s)</u>
MW-3P	$2.4 \times 10^{-4}$
MW-6P	$4.5 \times 10^{-4}$
MW-7P	$2.2 \times 10^{-3}$
MW-18P	$4.6 \times 10^{-4}$

ADAMS COUNTY LANDFILL  
FEASIBILITY STUDY PERMEABILITY TESTS  
SLUG TEST RESULTS: WELL 3P

Equation:  $K = \frac{r^2 \ln(L/R)}{2 L T_o}$

$r$  = well radius = 2.54 cm

$L$  = screen sand pack length = 228.60 cm

$R$  = borehole radius = 5.08 cm

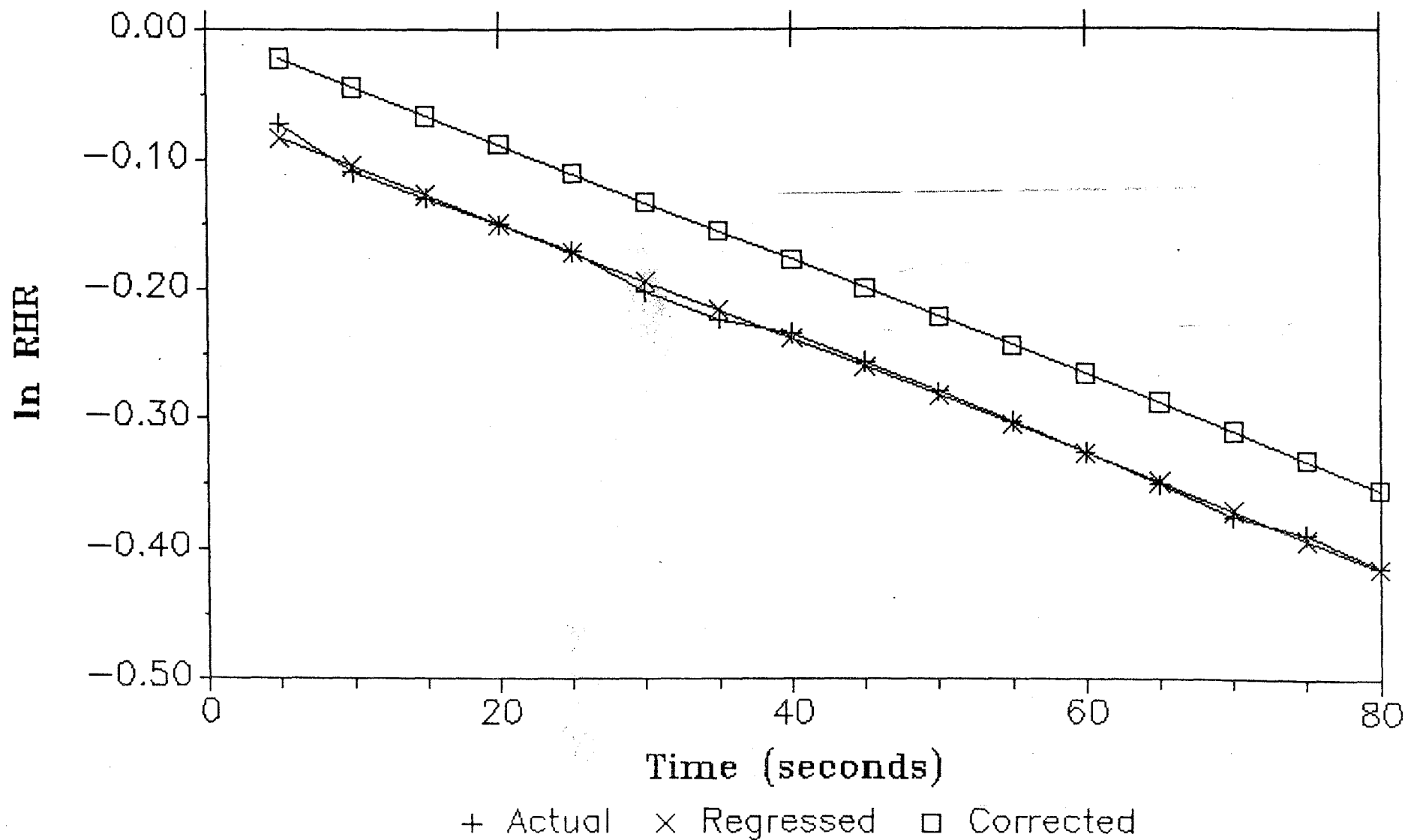
$H_o$  = initial head difference = 1.15 feet

$T_o$  = time lag = 224.8 seconds

--->  $K$  = hydraulic conductivity =  $2.4 \times 10^{-4}$  cm/second

Note:  $-T_o$  corresponds to the time when the natural log  
( $\ln$ ) of the residual head ratio is -1.00  
-RHR is the Residual Head Ratio which is the ratio  
of the unrecovered head difference ( $H$ ) and the  
initial head difference ( $H_o$ ) created by the  
added/removed water

ADAMS COUNTY LANDFILL  
Feasibility Study Permeability Tests  
Well MW-3P



Data From Slug Test



ADAMS COUNTY LANDFILL  
FEASIBILITY STUDY PERMEABILITY TESTS  
SLUG TEST RESULTS: WELL 6P

Equation:  $K = \frac{r^2 \ln(L/R)}{2 L T_o}$

r = well radius = 2.54 cm

L = screen sand pack length = 243.84 cm

R = borehole radius = 5.08 cm

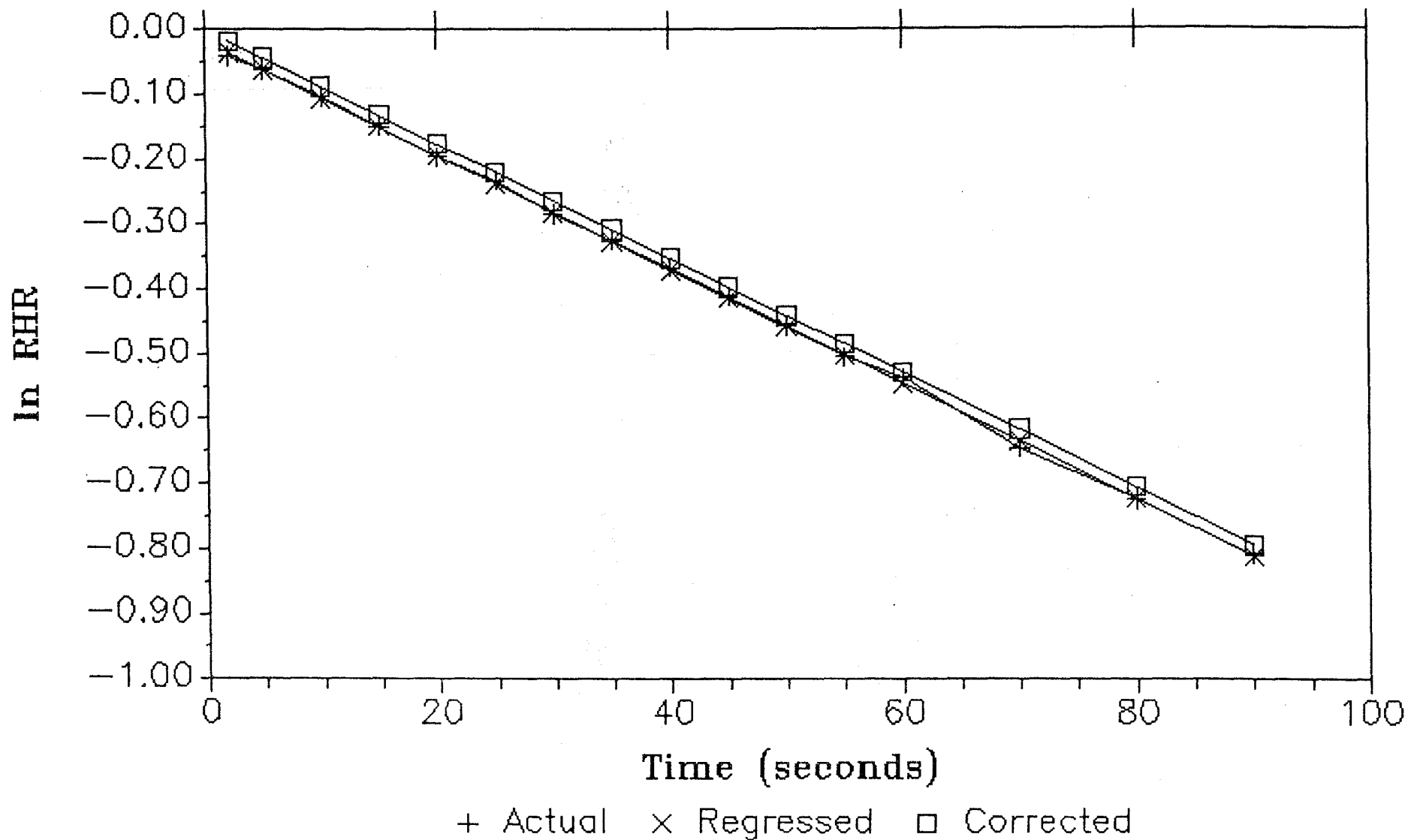
H<sub>o</sub> = initial head difference = 1.01 feet

T<sub>o</sub> = time lag = 112.9 seconds

---> K = hydraulic conductivity =  $4.5 \times 10^{-4}$  cm/second

Note: -T<sub>o</sub> corresponds to the time when the natural log  
(ln) of the residual head ratio is -1.00  
-RHR is the Residual Head Ratio which is the ratio  
of the unrecovered head difference (H) and the  
initial head difference (H<sub>o</sub>) created by the  
added/removed water

ADAMS COUNTY LANDFILL  
Feasibility Study Permeability Tests  
Well MW - 6P



Data From Slug Test

ADAMS COUNTY LANDFILL  
FEASIBILITY STUDY PERMEABILITY TESTS  
SLUG TEST RESULTS: WELL 7P

Equation:  $K = \frac{r^2 \ln(L/R)}{2 L T_o}$

$r$  = well radius = 2.54 cm

$L$  = screen sand pack length = 243.84 cm

$R$  = borehole radius = 5.08 cm

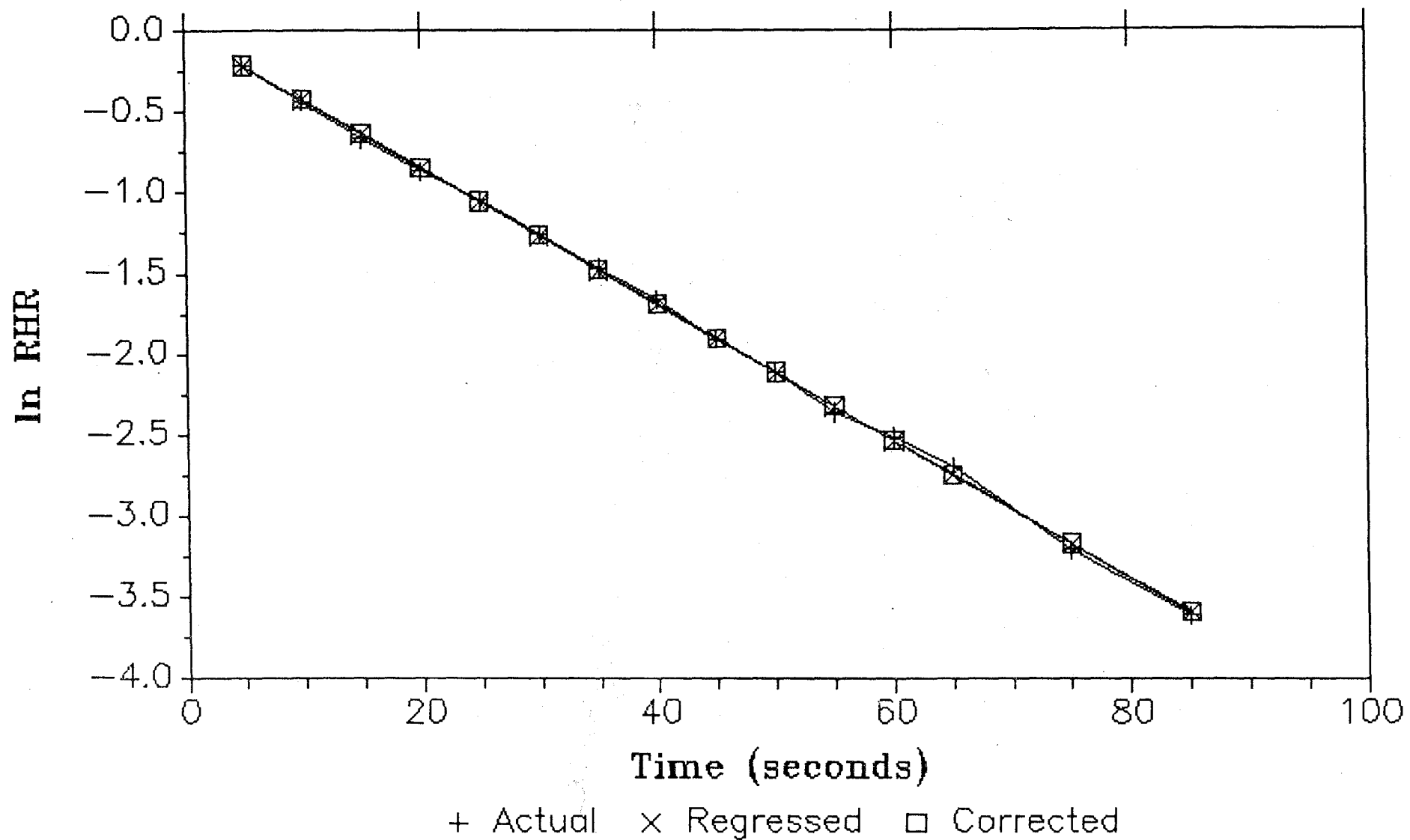
$H_o$  = initial head difference = 0.74 feet

$T_o$  = time lag = 23.6 seconds

--->  $K$  = hydraulic conductivity =  $2.2 \times 10^{-3}$  cm/second

Note:  $-T_o$  corresponds to the time when the natural log  
( $\ln$ ) of the residual head ratio is -1.00  
-RHR is the Residual Head Ratio which is the ratio  
of the unrecovered head difference ( $H$ ) and the  
initial head difference ( $H_o$ ) created by the  
added/removed water

ADAMS COUNTY LANDFILL  
Feasibility Study Permeability Tests  
Well MW - 7P



Data From Slug Test

ADAMS COUNTY LANDFILL  
FEASIBILITY STUDY PERMEABILITY TESTS  
SLUG TEST RESULTS: WELL 18P

Equation:  $K = \frac{r^2 \ln(L/R)}{2 L T_o}$

$r$  = well radius = 2.54 cm

$L$  = screen sand pack length = 228.60 cm

$R$  = borehole radius = 5.08 cm

$H_o$  = initial head difference = 1.39 feet

$T_o$  = time lag = 116.6 seconds

--->  $K$  = hydraulic conductivity =  $4.6 \times 10^{-4}$  cm/second

Note: - $T_o$  corresponds to the time when the natural log  
( $\ln$ ) of the residual head ratio is -1.00  
-RHR is the Residual Head Ratio which is the ratio  
of the unrecovered head difference ( $H$ ) and the  
initial head difference ( $H_o$ ) created by the  
added/removed water

ADAMS COUNTY LANDFILL  
Feasibility Study Permeability Tests  
Well MW-18P

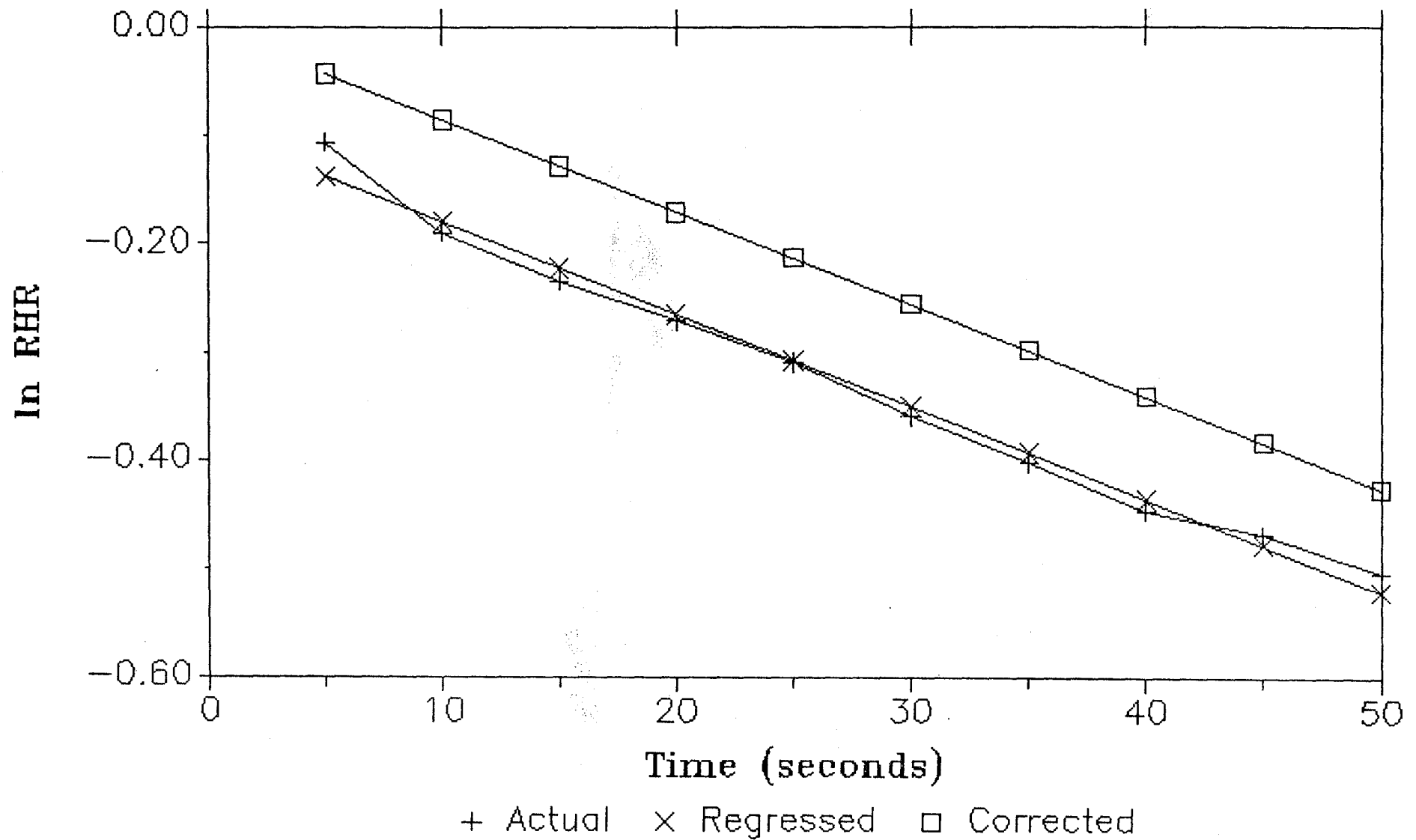


TABLE NO. 6-7

## IN-FIELD PERMEABILITY TESTS

Well	Hydraulic Conductivity (cm/sec)	Soil Type	Well Screen Elevation (USGS)
MW-1	$6.9 \times 10^{-2}$	SP;CL	935 - 920
MW-2	$1.1 \times 10^{-3}$	SP;CL	943 - 928
MW-3	$7.7 \times 10^{-3}$	SP;CL	938 - 923
MW-3P	$2.4 \times 10^{-4}$	SP	897 - 892
MW-6	$4.7 \times 10^{-3}$	SP;CL,ML	945 - 930
MW-6P	$4.5 \times 10^{-4}$	SP	907 - 902
MW-7	$4.1 \times 10^{-2}$	SM	943 - 933
MW-7P	$2.2 \times 10^{-3}$	SP	909 - 904
MW-8	$8.7 \times 10^{-3}$	SM;SP,CL	943 - 933
MW-9	$1.3 \times 10^{-2}$	SM;SP	942 - 932
MW-16	$1.6 \times 10^{-2}$	ML,CL,SM	945 - 935
MW-17	$5.4 \times 10^{-3}$	ML,CL,SM	943 - 933
MW-18	$1.6 \times 10^{-2}$	SP;ML,CL,SM	944 - 934
MW-18P	$4.6 \times 10^{-4}$	SP	908 - 903



# Foth & Van Dyke

Engineers/Architects

2737 S. Ridge Road

P. O. Box 19012

Green Bay, Wisconsin 54307-9012

414/497-2500

## FALLING/CONSTANT HEAD TEST

No. of Layers	
No. of Blows/Hammer Size	
Vol. of Water Added (c.c.)	
Wt. of Cyl. + Soil, Wm (lbs.)	
Wt. of Cyl., Wc (lbs.)	
Wt. of Soil, W (lbs.)	
Average Water Content, w(%)	
Moist Density, FM (lbs./ft. <sup>3</sup> )	
Dry Density, FM (dry) (lbs./ft. <sup>3</sup> )	
% Compaction	

JOB NO.:	86A22
BORING NO.:	10
SAMPLE NO.:	FR-17
DEPTH:	30-33'
TUBE DIAMETER	A = 2.80"
LENGTH OF SAMPLE	6.8125"
DIST. FROM TOP OF TUBE TO LOWER WATER LEVEL	26.3 cm
DATE:	July 18, 1986
TECH. NAME:	R. Rouse

	TIME AM/PM DATE	TIME INTERVAL (MIN.)	H @ START OF TEST	H @ FINISH	TARE	TOTAL WT. TARE + WATER, GR.	WEIGHT OF WATER, GR.	K CM/SEC.
(1)	08:05 AM/PM 7/18/86 16:08 AM/PM 7/18/86	(483) 28,980	SATURATION 101.0	96.1	201.7	299.8	98.1	$2.50 \times 10^{-6}$
(2)	16:08 AM/PM 7/18/86 10:37 AM/PM 7/21/86	(3985) 239,100	-- 96.1	83.3	201.7	436.7+	235.0+	$9.00 \times 10^{-7}$
(3)	10:37 AM/PM 7/21/86 07:32 AM/PM 7/22/86	(1255) 75,300	@ 2 psi 83.3	74.6	201.7	379.8	178.1	$8.00 \times 10^{-7}$
(4)	07:32 AM/PM 7/22/86 07:11 AM/PM 7/23/86	(1419) 85,140	-- 74.6	72.2	201.7	246.4	44.7	$5.00 \times 10^{-7}$
(5)	07:11 AM/PM 7/23/86 22:58 AM/PM 7/26/86	(5267) 316,020	-- 72.2	66.3	201.7	312.6	110.9	$4.00 \times 10^{-7}$
(6)	22:58 AM/PM 7/26/86 09:43 AM/PM 7/29/86	(3525) 211,500	66.3	62.9	201.7	260.7	59.0	$4.00 \times 10^{-7}$
(7)	09:43 AM/PM 7/29/86 14:33 AM/PM 8/04/86	(8930) 535,800	@ 2 psi 62.9	55.7	201.7	330.1	128.4	$9.61 \times 10^{-8}$
(8)	14:33 AM/PM 8/04/86 11:43 AM/PM 8/10/86	(8470) 508,200	@ 1 psi 55.7	49.4	201.7	310.0	108.3	$1.00 \times 10^{-7}$
(9)	11:43 AM/PM 8/10/86 07:38 AM/PM 8/12/86	(2635) 158,100	@ 1 psi 49.4	47.7	201.7	231.0	29.3	$1.00 \times 10^{-7}$
(10)	07:38 AM/PM 8/12/86 13:10 AM/PM 8/18/86	(8972) 538,320	@ 1 psi 47.7	41.2	201.7	318.7	117.0	$2.00 \times 10^{-7}$
(11)	13:10 AM/PM 8/18/86 09:20 AM/PM 8/21/86	(4090) 245,400	@ 1 psi 41.2	38.2	201.7	251.9	50.2	$2.00 \times 10^{-7}$
(12)	09:20 AM/PM 8/21/86 09:20 AM/PM 8/25/86	(5760) 345,600	@ 1 psi 38.2	34.3	201.7	--	--	$2.00 \times 10^{-7}$
	AM/PM							
	AM/PM							
	AM/PM					Perm Rate		$2 \times 10^{-7}$
	AM/PM							

# Foth & Van Dyke

Engineers/Architects

2737 S. Ridge Road  
P. O. Box 19012  
Green Bay, Wisconsin 54307-9012  
414/497-2500

PROJECT: Adams County Feasibility

JOB NO.: 86A22

DATE: September 11, 1986

## PERMEABILITY TEST CONSTANT HEAD

SAMPLE NO.: FR-25 - Boring #11 at 10' to 15' depth

SOIL DESCRIPTION: SAND, fine to medium grained, light brown (SP)

% COMPACTION --

COMPACTED DRY DENSITY = 103.3 pcf

MOISTURE = 7.4%

SAMPLE DIAMETER = 4.00"

SAMPLE HEIGHT = 4.5625" (4-9/16")

RUN NO.	(CM)	(Seconds)	PERMEABILITY, CM/SEC.	REMARKS
	HEAD, <del>INCHES</del>	DURATION, <del>MINUTES</del>		
1	83.0	15	$1.06 \times 10^{-2}$	
2	83.0	15	$1.03 \times 10^{-2}$	
3	83.0	15	$1.03 \times 10^{-2}$	
4	83.0	15	$1.05 \times 10^{-2}$	
5	83.0	15	$1.04 \times 10^{-2}$	
Average for Test			$1.04 \times 10^{-2}$	
Perm Rate			$1 \times 10^{-2}$	

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PROJECT: Adams County Feasibility

JOB NO.: 86A22

DATE: September 11, 1986

## PERMEABILITY TEST CONSTANT HEAD

SAMPLE NO.: FR-21 - Boring #12 at 5' to 10' depth

SOIL DESCRIPTION: SILTY SAND, fine grained, light brown (SM)

% COMPACTION 92

COMPACTED DRY DENSITY = 106.7 pcf

MOISTURE = 10.4%

SAMPLE DIAMETER = 4.0"

SAMPLE HEIGHT = 4.5625"

<u>RUN NO.</u>	<u>HEAD, <sup>(CM)</sup> <del>INCHES</del></u>	<u>DURATION, <sup>(Seconds)</sup> <del>MINUTES</del></u>	<u>PERMEABILITY, CM/SEC.</u>	<u>REMARKS</u>
1	84.5	30	$6.60 \times 10^{-4}$	
2	84.5	30	$6.43 \times 10^{-4}$	
3	84.5	30	$6.77 \times 10^{-4}$	
4	84.5	30	$6.77 \times 10^{-4}$	
5	84.5	30	$6.43 \times 10^{-4}$	
Average of Tests			$6.60 \times 10^{-4}$	
Perm Rate			$7 \times 10^{-4}$	

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## FALLING/CONSTANT HEAD TEST

No. of Layers	
No. of Blows/Hammer Size	
Vol. of Water Added (c.c.)	
Wt. of Cyl. + Soil, Wm (lbs.)	
Wt. of Cyl., Wc (lbs.)	
Wt. of Soil, W (lbs.)	
Average Water Content, w(%)	
Moist Density, FM (lbs./ft. <sup>3</sup> )	
Dry Density, FM (dry) (lbs./ft. <sup>3</sup> )	
% Compaction	

JOB NO.:	86A22
BORING NO.:	12
SAMPLE NO.:	FR-16
DEPTH:	32'
TUBE DIAMETER	A = 2.80"
LENGTH OF SAMPLE	7.0"
DIST. FROM TOP OF TUBE TO LOWER WATER LEVEL	26.0 cm
DATE:	July 16, 1986
TECH. NAME:	R. Rouse

	TIME AM/PM DATE	TIME INTERVAL (MIN.)	H @ START OF TEST	H @ FINISH	TARE	TOTAL WT. TARE + WATER, GR.	WEIGHT OF WATER, GR.	K CM/SEC.
	16:25 AM/PM 7/16/86	--	SATURATION					
	AM/PM		102.8	--	207.3	--	--	
(1)	12:35 AM/PM 7/17/86	(1657)						
	16:12 AM/PM 7/18/86	99,420	102.4	102.0	207.3	220.4	13.1	$5.79 \times 10^{-8}$
(2)	16:12 AM/PM 7/18/86	(3986)						
	10:38 AM/PM 7/21/86	239,160	102.0	101.2	207.3	217.1	9.8	$4.84 \times 10^{-8}$
(3)	10:38 AM/PM 7/21/86	(2675)						
	07:13 AM/PM 7/23/86	160,500	101.2	99.0	207.3	242.9	35.6	$2.00 \times 10^{-7}$
(4)	07:13 AM/PM 7/23/86	(4546)						
	10:59 AM/PM 7/26/86	272,760	99.0	94.4	207.3	288.9	81.6	$3.00 \times 10^{-7}$
(5)	10:59 AM/PM 7/26/86	(4245)						
	09:44 AM/PM 7/29/86	254,700	94.4	91.6	207.3	260.6	53.3	$2.00 \times 10^{-7}$
(6)	09:44 AM/PM 7/29/86	(8931)						
	14:35 AM/PM 8/04/86	535,860	91.6	84.6	207.3	329.6	122.3	$2.00 \times 10^{-7}$
(7)	14:35 AM/PM 8/04/86	(8470)						
	11:45 AM/PM 8/10/86	508,200	84.6	78.4	207.3	317.4	110.1	$2.00 \times 10^{-7}$
(8)	11:45 AM/PM 8/10/86	(2635)						
	07:40 AM/PM 8/12/86	158,100	78.4	76.5	207.3	239.3	32.0	$2.00 \times 10^{-7}$
(9)	07:40 AM/PM 8/12/86	(8956)						
	12:56 AM/PM 8/18/86	537,370	76.5	70.3	207.3	317.2	109.9	$2.00 \times 10^{-7}$
(10)	12:56 AM/PM 8/18/86	(4120)						
	09:36 AM/PM 8/21/86	247,200	70.3	67.4	207.3	255.3	48.0	$3.00 \times 10^{-7}$
(11)	09:36 AM/PM 8/21/86	(5794)						
	10:10 AM/PM 8/25/86	347,640	67.4	63.7	207.3	--	--	$2.00 \times 10^{-7}$
	AM/PM							
	AM/PM							
	AM/PM							
	AM/PM							
						Perm Rate		$2 \times 10^{-7}$

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2737 S. Ridge Road

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PROJECT: Adams County Study

JOB NO.: 86A22

DATE: September 10, 1986

## PERMEABILITY TEST CONSTANT HEAD

SAMPLE NO.: FR-20

Boring #13 at 10' - 13' depth

SOIL DESCRIPTION: Sand, fine grained, brown (SP)

% COMPACTION = 91 1/2

COMPACTED DRY DENSITY = 101.7 pct

MOISTURE = 5.6%

SAMPLE DIAMETER = 4.00"

SAMPLE HEIGHT = 4.5625" (4 9/16")

<u>RUN NO.</u>	<u>HEAD, <sup>CM</sup> <del>INCHES</del></u>	<u>DURATION, <sup>Seconds</sup> <del>MINUTES</del></u>	<u>PERMEABILITY, CM/SEC.</u>	<u>REMARKS</u>
1	82.1	15	$7.66 \times 10^{-3}$	
2	82.1	15	$7.37 \times 10^{-3}$	
3	82.1	15	$7.40 \times 10^{-3}$	
4	82.1	15	$7.31 \times 10^{-3}$	
5	82.1	15	$7.09 \times 10^{-3}$	

Average of Tests =  $7.37 \times 10^{-3}$

## Engineers/Architects

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## FALLING/CONSTANT HEAD TEST

Recompacted Perm

No. of Layers	4
No. of Blows/Hammer Size	25/10#
Vol. of Water Added (c.c.)	
Wt. of Cyl. + Soil, Wm (lbs.)	5409
Wt. of Cyl., Wc (lbs.)	3357
Wt. of Soil, W (lbs.)	2052
Average Water Content, w(%)	11.1
Moist Density, FM (lbs./ft. <sup>3</sup> )	135.7
Dry Density, FM (dry) (lbs./ft. <sup>3</sup> )	122.2
% Compaction	95

JOB NO.:	86A22 FR
BORING NO.:	MW-8
SAMPLE NO.:	
DEPTH:	50-55'
TUBE DIAMETER	A = 4.0"
LENGTH OF SAMPLE	4.50'
DIST. FROM TOP OF TUBE TO LOWER WATER LEVEL	33.2 cm
DATE:	September 13-19, 1986
TECH. NAME:	RRR

[illegible]

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PROJECT: Adams County Study

JOB NO.: 86A22 FR

DATE: September 10, 1986

## PERMEABILITY TEST CONSTANT HEAD

SAMPLE NO.: FR-19 Boring MW-9 at 10' depth

SOIL DESCRIPTION: Sand, fine grained, brown (SP)

% COMPACTION - 90

COMPACTED DRY DENSITY = 100.1 pct

MOISTURE = 1.7%

SAMPLE DIAMETER = 4.00"

SAMPLE HEIGHT = 4.5625 (4 9/16")

<u>RUN NO.</u>	<u>HEAD, <sup>CM.</sup> <del>INCHES</del></u>	<u>DURATION, <sup>Seconds</sup> <del>MINUTES</del></u>	<u>PERMEABILITY, CM/SEC.</u>	<u>REMARKS</u>
1	82.7 cm	15	$8.54 \times 10^{-3}$	
2	82.7 cm	15	$8.49 \times 10^{-3}$	
3	82.7 cm	15	$8.47 \times 10^{-3}$	
4	82.7 cm	15	$7.95 \times 10^{-3}$	
5	82.7 cm	15	$7.88 \times 10^{-3}$	
Average of Tests =			$8.27 \times 10^{-3}$	