

Appendix D
Field Hydraulic Conductivity Testing

Hydraulic Conductivity Testing

Hydraulic conductivity (slug) tests were performed on each of the four new monitoring wells installed at the site for the feasibility study, including water table wells MW-29, MW-30, and MW-31 and piezometer MW-30P. The slug tests were performed by rapidly lowering a solid cylinder (slug) into the well to cause an instantaneous rise in water level (falling head test), then measuring the return of the water level to its static condition. A second test was performed by removing the slug (rising head test), and again measuring the response of the water level in the well. Water level data were recorded with an In-Situ, Inc. automated pressure transducer (Level TROLL 700) and data logger system. Slug test data were evaluated using Waterloo Hydrologic Aquifer Test Pro v. 2013.1 graphical analysis and reporting software. The slug tests were analyzed using the methods of Bouwer and Rice (1976)¹ for unconfined aquifers.

Hydraulic conductivity values (recovery test only) calculated for water table observation wells ranged from 1.1×10^{-2} cm/sec in well MW-29, screened primarily in silty sand, silt and clay deposits, to 1.4×10^{-3} cm/sec in well MW-31, screened in silty sand and clay deposits. The hydraulic conductivity value calculated for the piezometer, which is screened in silty sand, was 2.1×10^{-2} cm/sec.

¹ Bouwer, H. and R.C. Rice, A Slug Test for Determining Hydraulic Conductivity of Unconfined Aquifers with Completely or Partially Penetrating Wells, *Water Resources Research*, Vol.12, No.3, 1976, pp.423-428

Table
Summary of Slug Test Parameters
Adams County Landfill

| Well Number | Test Number | Depth of Well (ft) | Depth to Water (ft) | Initial Drawdown Elevation (t_0) (ft) | Internal Well Radius (r) (ft) | Effective Well Radius (R) (ft) | Sat. Aquifer Thickness (ft) | Screen Length (L) (ft) | Height of Water Column (b) (ft) |
|-------------|-------------|--------------------|---------------------|---|-----------------------------------|------------------------------------|-----------------------------|------------------------|---------------------------------|
| MW-29 | Slug In | 34.1 | 24.76 | 24.95 | 0.083 | 0.33 | 9.34 | 10 | 9.34 |
| | Slug Out | | | 22.76 | | | | | |
| MW-30 | Slug In | 46.9 | 38.48 | 39.03 | 0.083 | 0.33 | 8.42 | 9 | 8.42 |
| | Slug Out | | | 37.77 | | | | | |
| MW-30P | Slug In | 75.8 | 44.22 | 46.4 | 0.083 | 0.33 | 32 | 5 | 31.58 |
| | Slug Out | | | 42.36 | | | | | |
| MW-31 | Slug In | 41.4 | 32.70 | 33.15 | 0.083 | 0.33 | 8.70 | 9 | 8.70 |
| | Slug Out | | | 30.59 | | | | | |



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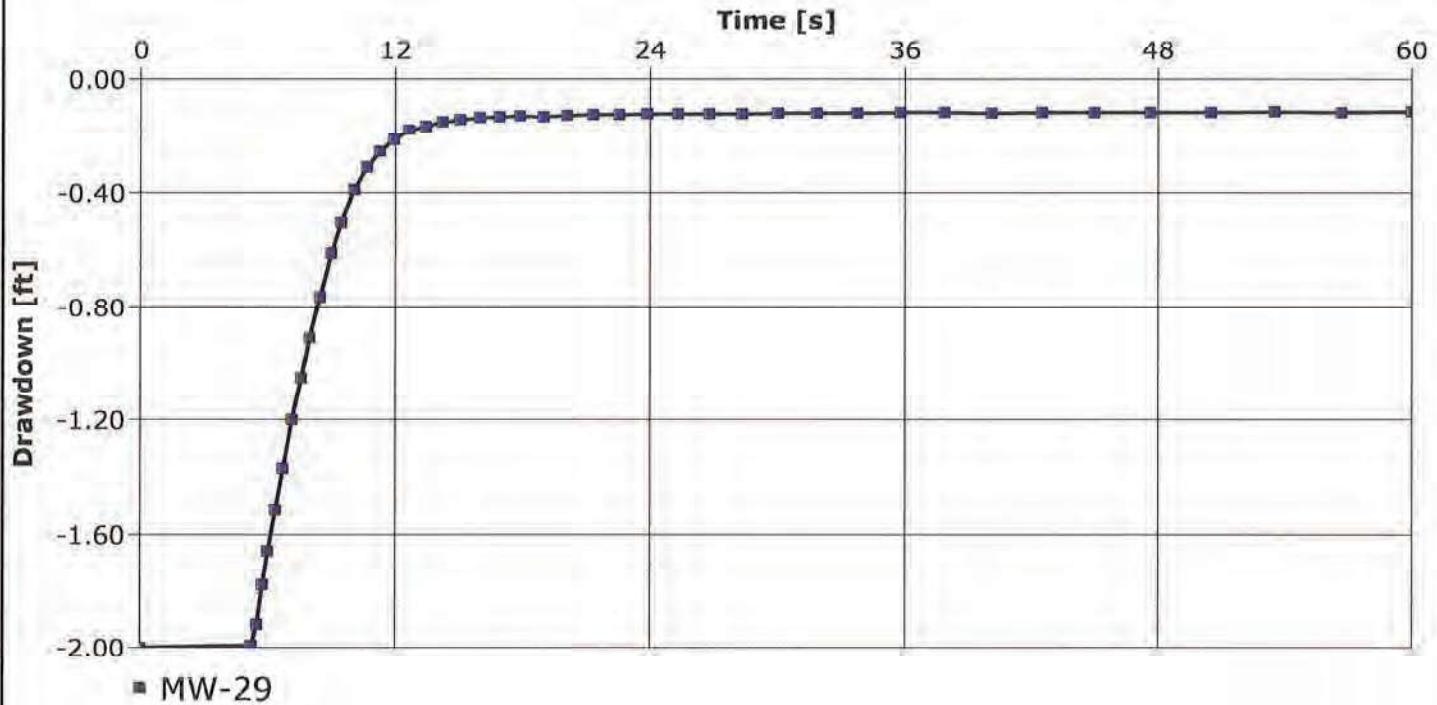
Slug Test Analysis Report

Project: Adams County Landfill

Number: 10-1070.12

Client: Adams County Solid Waste Department

| | | |
|-------------------------------------|------------------------------|--------------------------|
| Location: Adams, WI | Slug Test: MW-29 Slug Out | Test Well: MW-29 |
| Test Conducted by: Jeff Steiner | | Test Date: 1/28/2016 |
| Analysis Performed by: Jeff Steiner | MW-29 Slug Out Time-Drawdown | Analysis Date: 1/29/2016 |
| Aquifer Thickness: 10.00 ft | | |





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Slug Test Analysis Report

Project: Adams County Landfill

Number: 10-1070.12

Client: Adams County Solid Waste Department

Location: Adams, WI

Slug Test: MW-29 Slug Out

Test Well: MW-29

Test Conducted by: Jeff Steiner

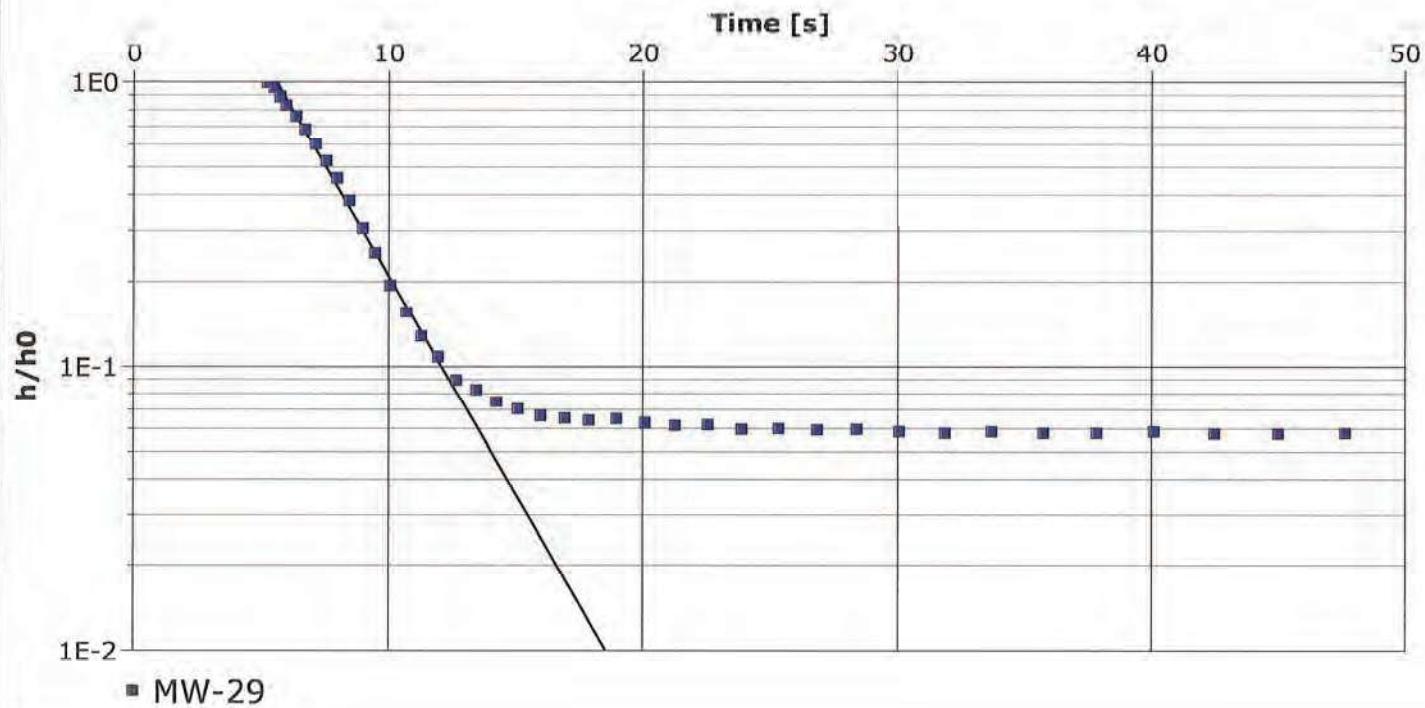
Test Date: 1/28/2016

Analysis Performed by: Jeff Steiner

MW-29 Slug Out Bouwer & Rice

Analysis Date: 1/29/2016

Aquifer Thickness: 10.00 ft



Calculation using Bouwer & Rice

| Observation Well | Hydraulic Conductivity [ft/s] | |
|------------------|----------------------------------|--|
| MW-29 | 3.80×10^{-4} | |



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Slug Test Analysis Report

Project: Adams County Landfill

Number: 10-1070.12

Client: Adams County Solid Waste Department

Location: Adams, WI

Slug Test: MW-30 Slug In

Test Well: MW-30

Test Conducted by: Jeff Steiner

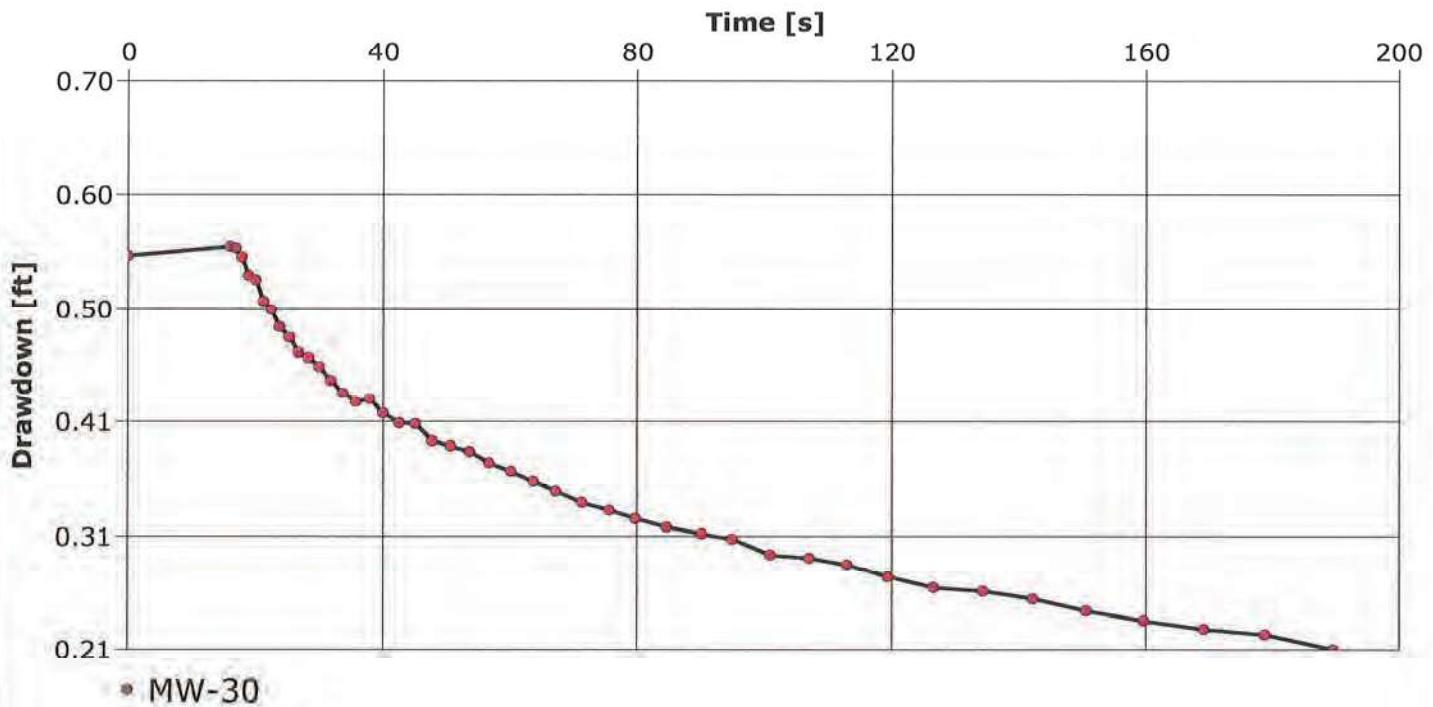
Test Date: 1/28/2016

Analysis Performed by: Jeff Steiner

MW-30 Slug In Time-Drawdown

Analysis Date: 1/29/2016

Aquifer Thickness: 8.42 ft





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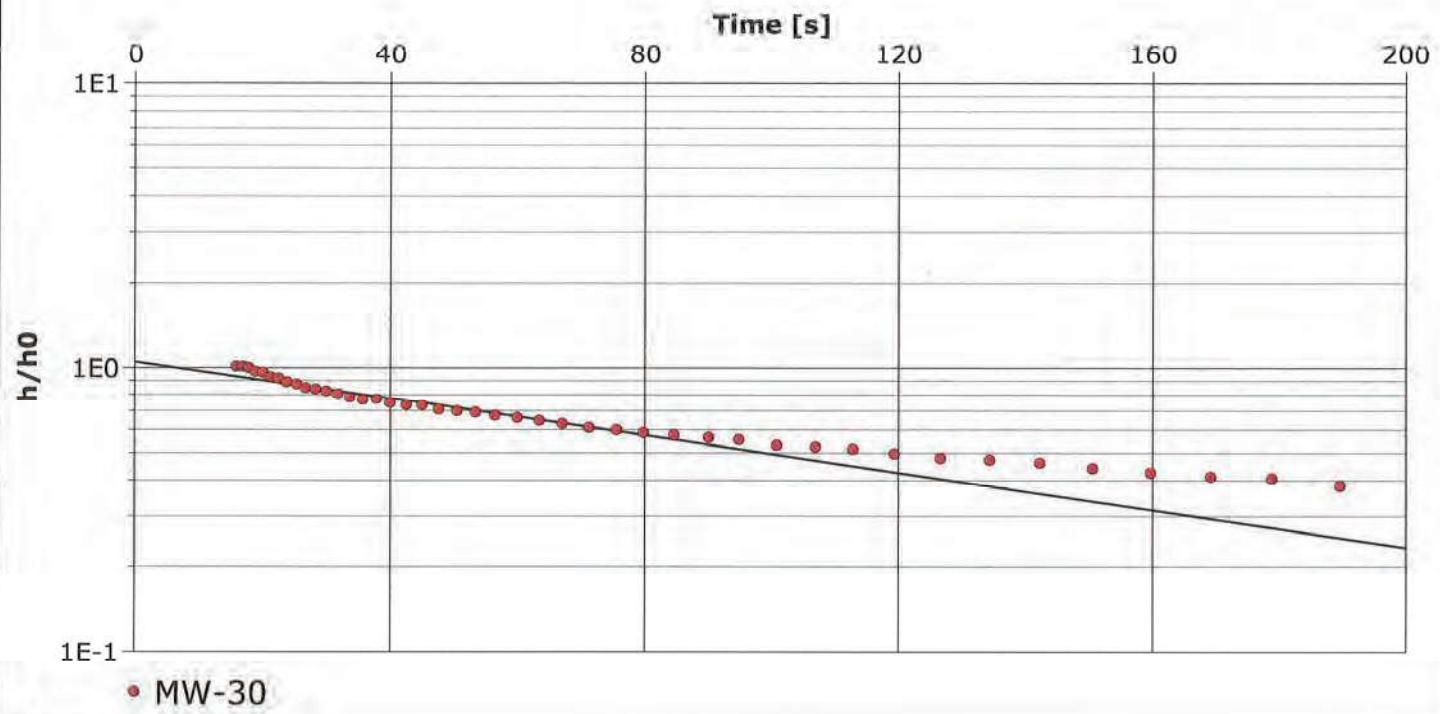
Slug Test Analysis Report

Project: Adams County Landfill

Number: 10-1070.12

Client: Adams County Solid Waste Department

| | | |
|-------------------------------------|-----------------------------|--------------------------|
| Location: Adams, WI | Slug Test: MW-30 Slug In | Test Well: MW-30 |
| Test Conducted by: Jeff Steiner | | Test Date: 1/28/2016 |
| Analysis Performed by: Jeff Steiner | MW-30 Slug In Bouwer & Rice | Analysis Date: 1/29/2016 |
| Aquifer Thickness: 8.42 ft | | |



• MW-30

Calculation using Bouwer & Rice

| Observation Well | Hydraulic Conductivity [ft/s] | |
|------------------|----------------------------------|--|
| MW-30 | 8.68×10^{-6} | |



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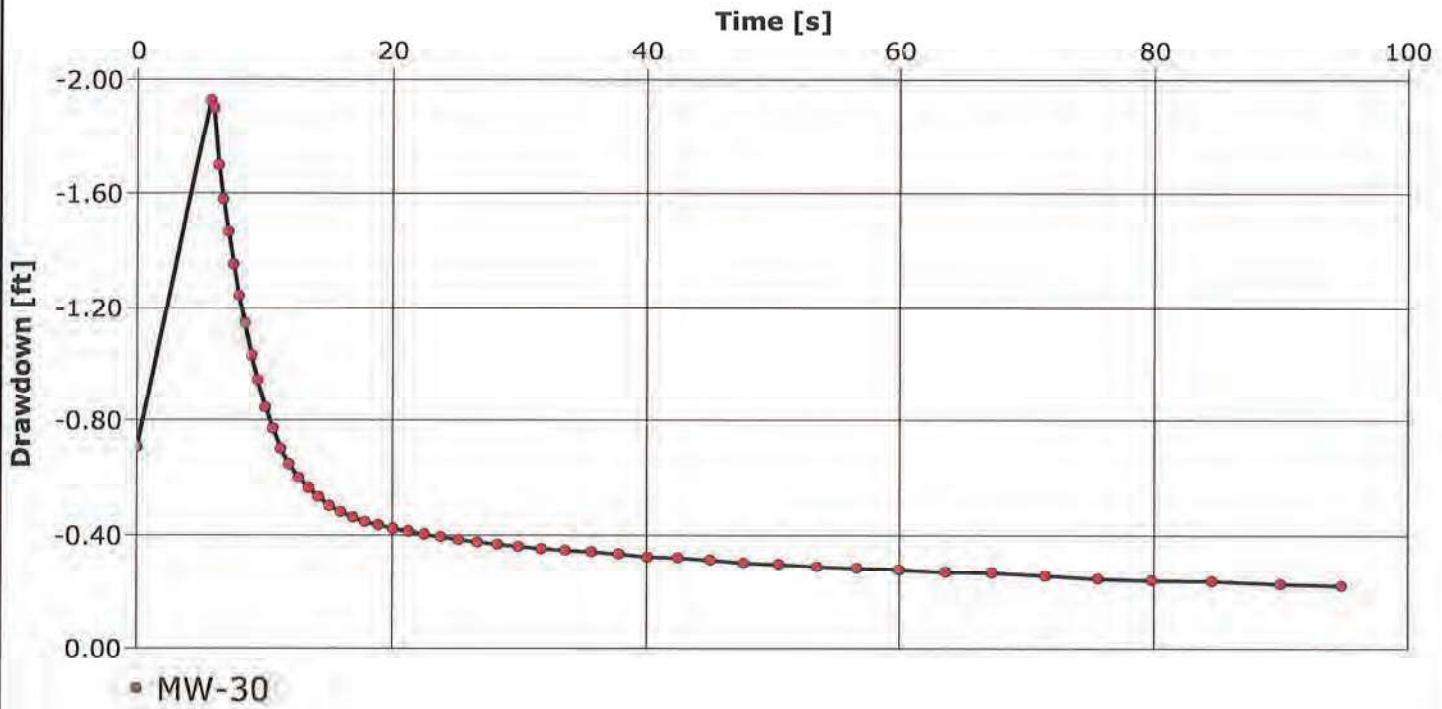
Slug Test Analysis Report

Project: Adams County Landfill

Number: 10-1070.12

Client: Adams County Solid Waste Department

| | | |
|-------------------------------------|------------------------------|--------------------------|
| Location: Adams, WI | Slug Test: MW-30 Slug Out | Test Well: MW-30 |
| Test Conducted by: Jeff Steiner | Test Date: 1/28/2016 | |
| Analysis Performed by: Jeff Steiner | MW-30 Slug Out Time-Drawdown | Analysis Date: 1/29/2016 |
| Aquifer Thickness: 8.42 ft | | |





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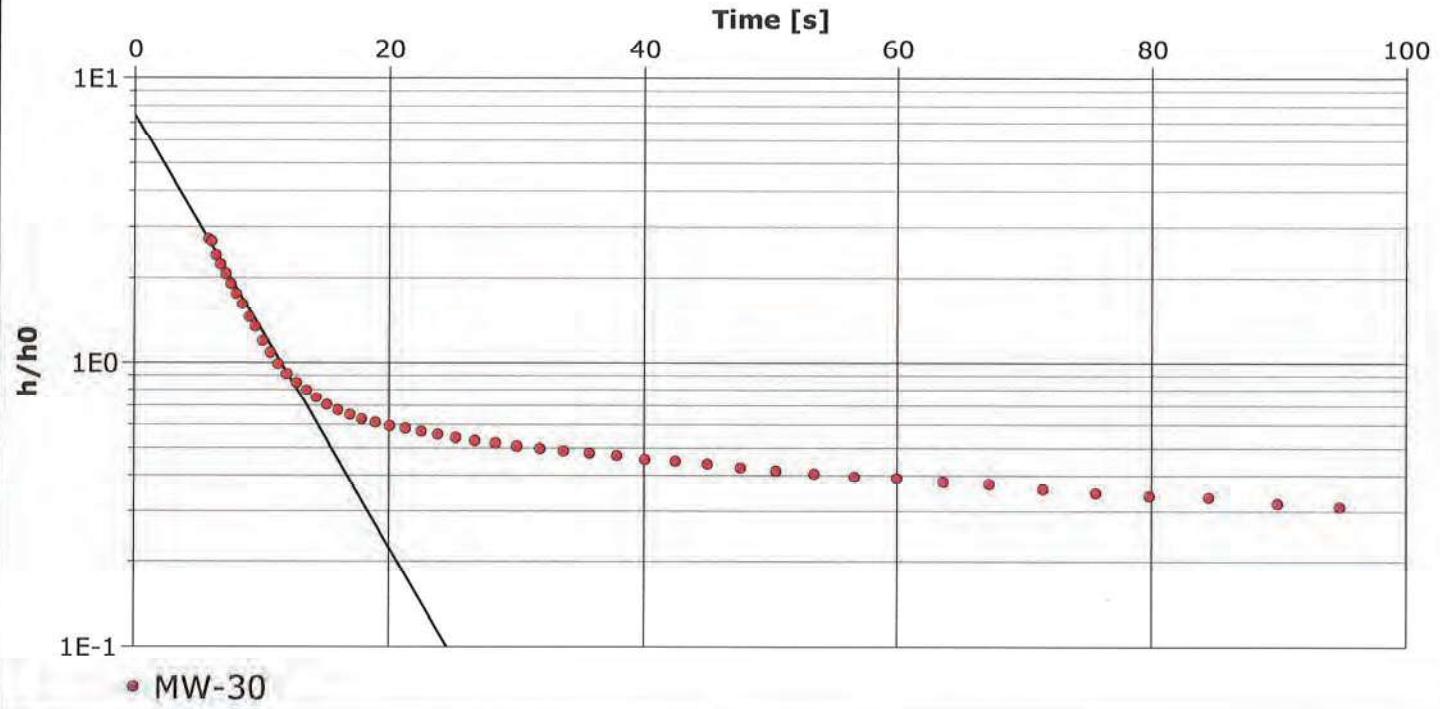
Slug Test Analysis Report

Project: Adams County Landfill

Number: 10-1070.12

Client: Adams County Solid Waste Department

| | | |
|-------------------------------------|------------------------------|--------------------------|
| Location: Adams, WI | Slug Test: MW-30 Slug Out | Test Well: MW-30 |
| Test Conducted by: Jeff Steiner | | Test Date: 1/28/2016 |
| Analysis Performed by: Jeff Steiner | MW-30 Slug Out Bouwer & Rice | Analysis Date: 1/29/2016 |
| Aquifer Thickness: 8.42 ft | | |



Calculation using Bouwer & Rice

| Observation Well | Hydraulic Conductivity [ft/s] | |
|------------------|----------------------------------|--|
| MW-30 | 2.02×10^{-4} | |



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Slug Test Analysis Report

Project: Adams County Landfill

Number: 10-1070.12

Client: Adams County Solid Waste Department

Location: Adams, WI

Slug Test: MW-30P Slug In

Test Well: MW-30P

Test Conducted by: Jeff Steiner

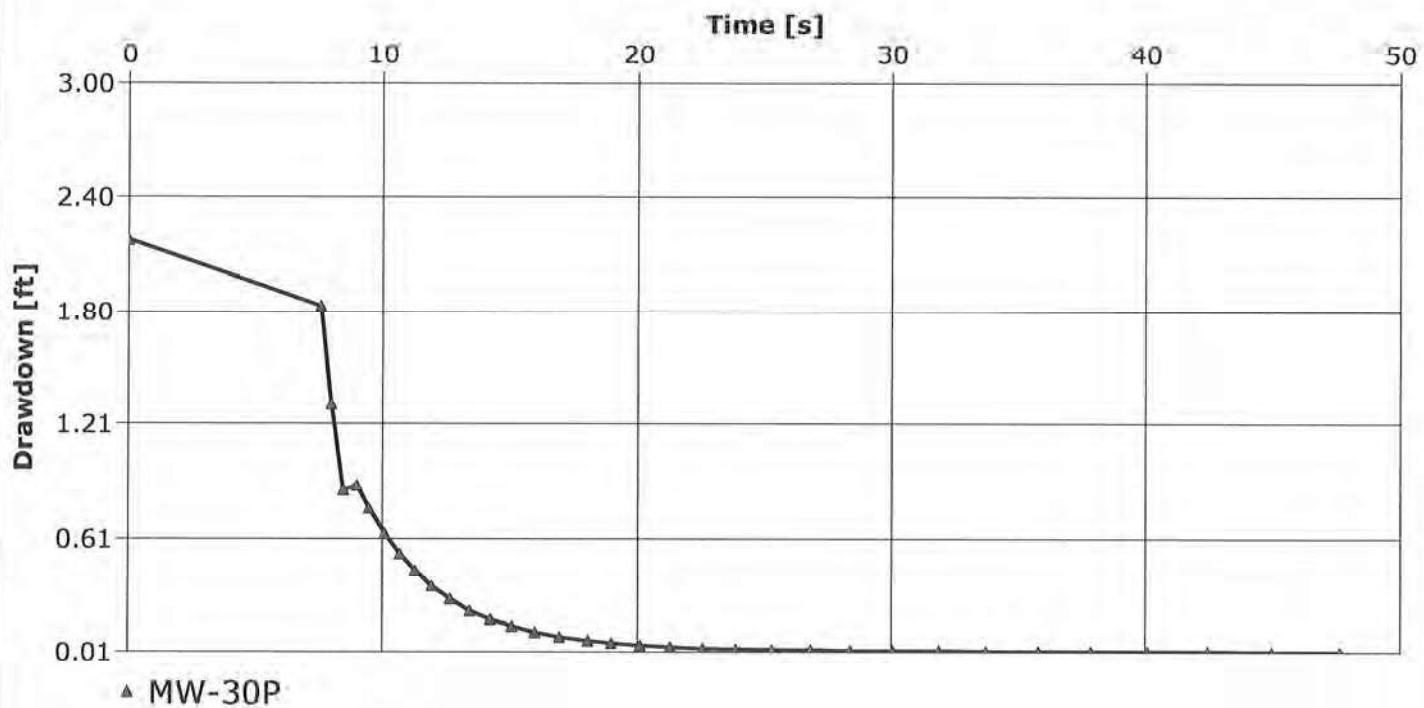
Test Date: 1/28/2016

Analysis Performed by: Jeff Steiner

MW-30P Slug In Time-Drawdown

Analysis Date: 1/29/2016

Aquifer Thickness: 32.00 ft





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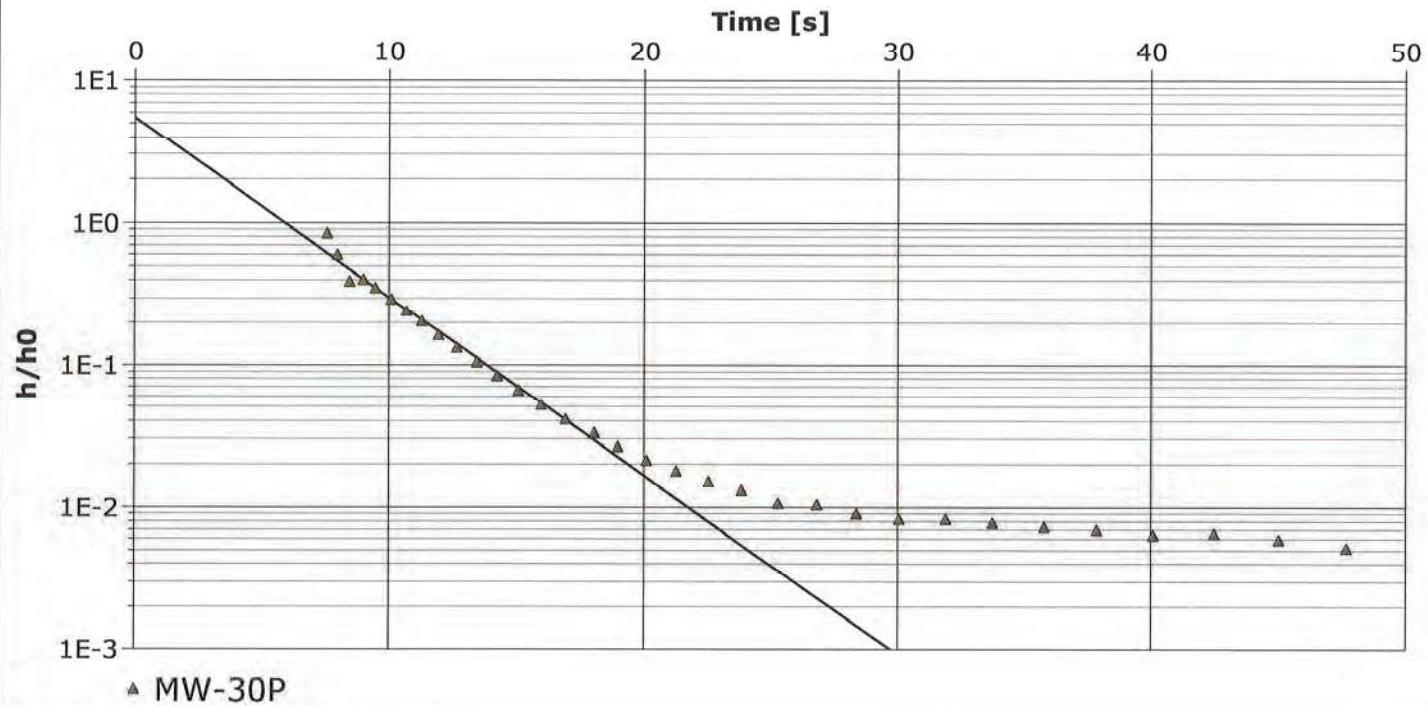
Slug Test Analysis Report

Project: Adams County Landfill

Number: 10-1070.12

Client: Adams County Solid Waste Department

| | | |
|-------------------------------------|-----------------------------|--------------------------|
| Location: Adams, WI | Slug Test: MW-30P Slug In | Test Well: MW-30P |
| Test Conducted by: Jeff Steiner | | Test Date: 1/28/2016 |
| Analysis Performed by: Jeff Steiner | MW-30 Slug In Bouwer & Rice | Analysis Date: 1/29/2016 |
| Aquifer Thickness: 32.00 ft | | |



Calculation using Bouwer & Rice

| Observation Well | Hydraulic Conductivity [ft/s] | |
|------------------|----------------------------------|--|
| MW-30P | 6.31×10^{-4} | |



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Slug Test Analysis Report

Project: Adams County Landfill

Number: 10-1070.12

Client: Adams County Solid Waste Department

Location: Adams, WI

Slug Test: MW-30P Slug Out

Test Well: MW-30P

Test Conducted by: Jeff Steiner

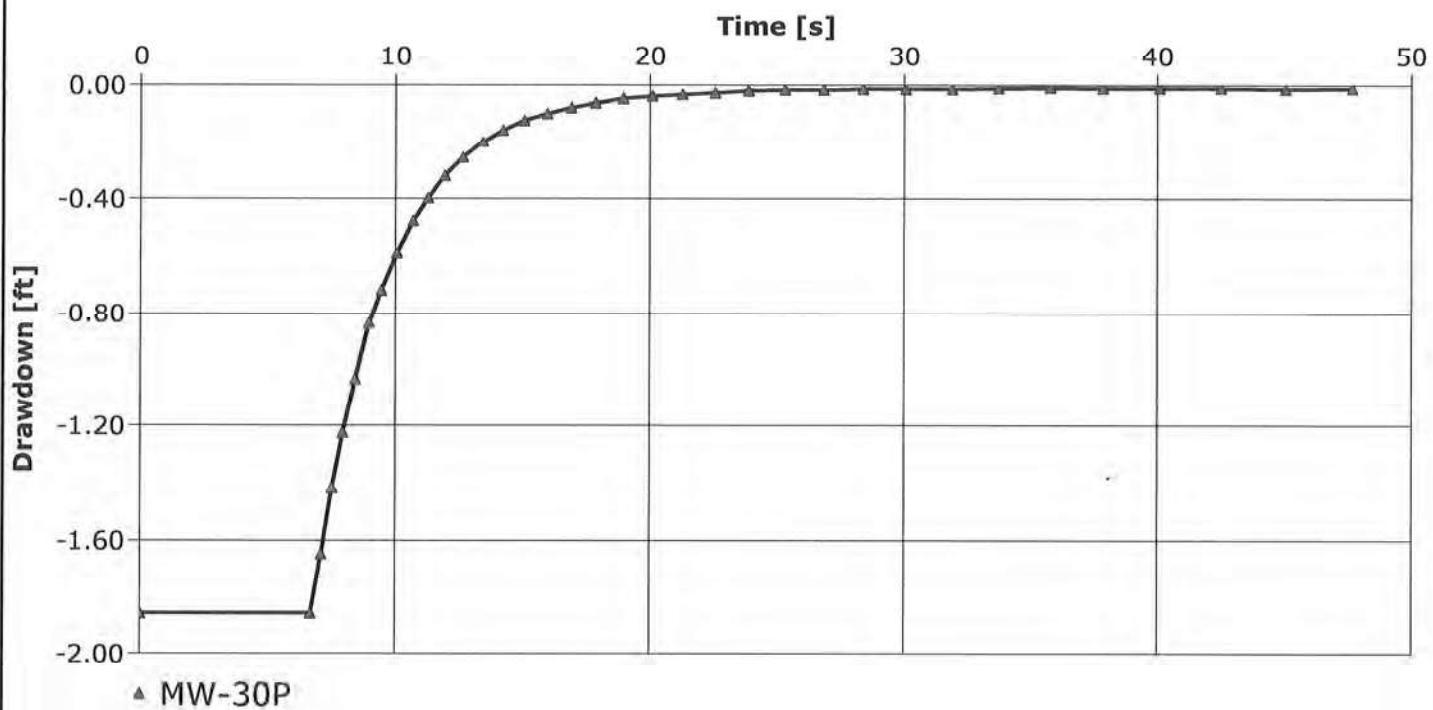
Test Date: 1/28/2016

Analysis Performed by: Jeff Steiner

MW-30P Slug Out

Analysis Date: 1/29/2016

Aquifer Thickness: 32.00 ft





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Slug Test Analysis Report

Project: Adams County Landfill

Number: 10-1070.12

Client: Adams County Solid Waste Department

Location: Adams, WI

Slug Test: MW-30P Slug Out

Test Well: MW-30P

Test Conducted by: Jeff Steiner

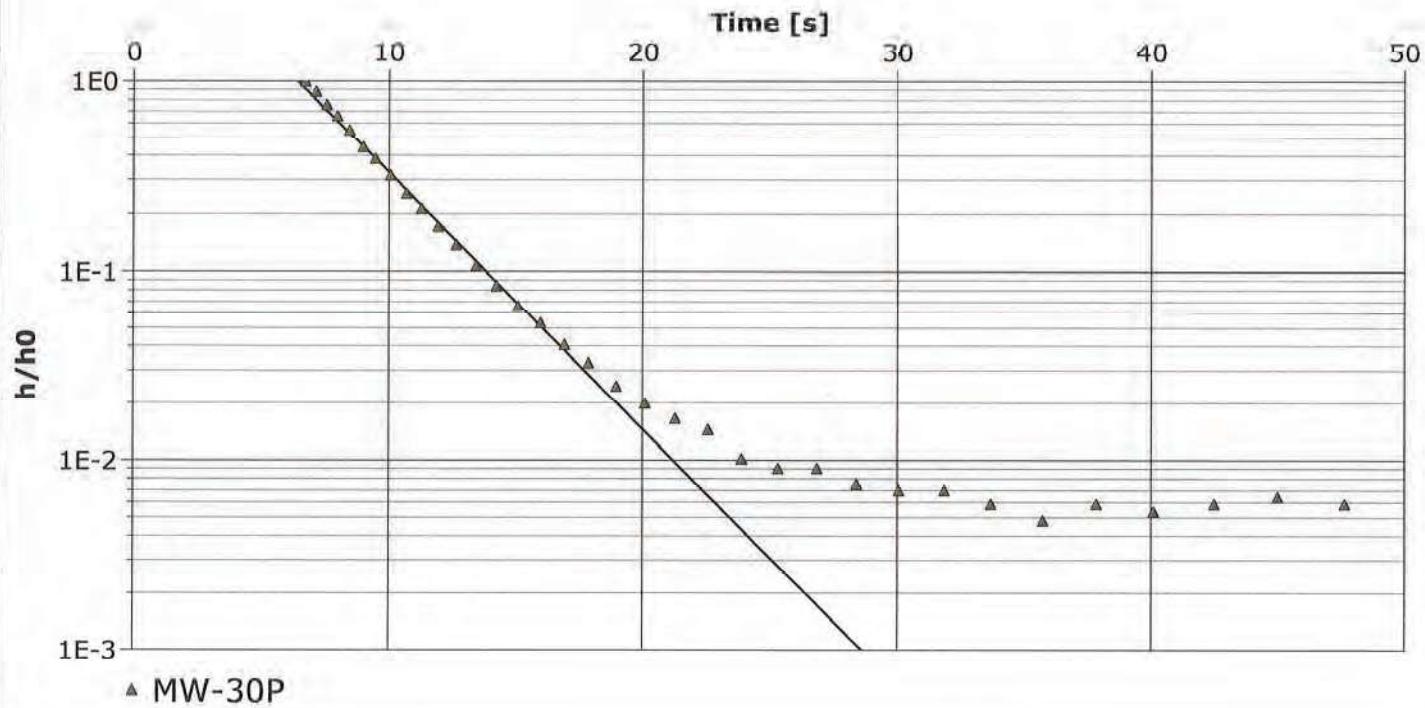
Test Date: 1/28/2016

Analysis Performed by: Jeff Steiner

MW-30P Slug Out Bouwer & Rice

Analysis Date: 1/29/2016

Aquifer Thickness: 32.00 ft



Calculation using Bouwer & Rice

| Observation Well | Hydraulic Conductivity [ft/s] | |
|------------------|----------------------------------|--|
| MW-30P | 6.79×10^{-4} | |


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Slug Test Analysis Report

Project: Adams County Landfill

Number: 10-1070.12

Client: Adams County Solid Waste Department

Location: Adams, WI

Slug Test: MW-31 Slug In

Test Well: MW-31

Test Conducted by: Jeff Steiner

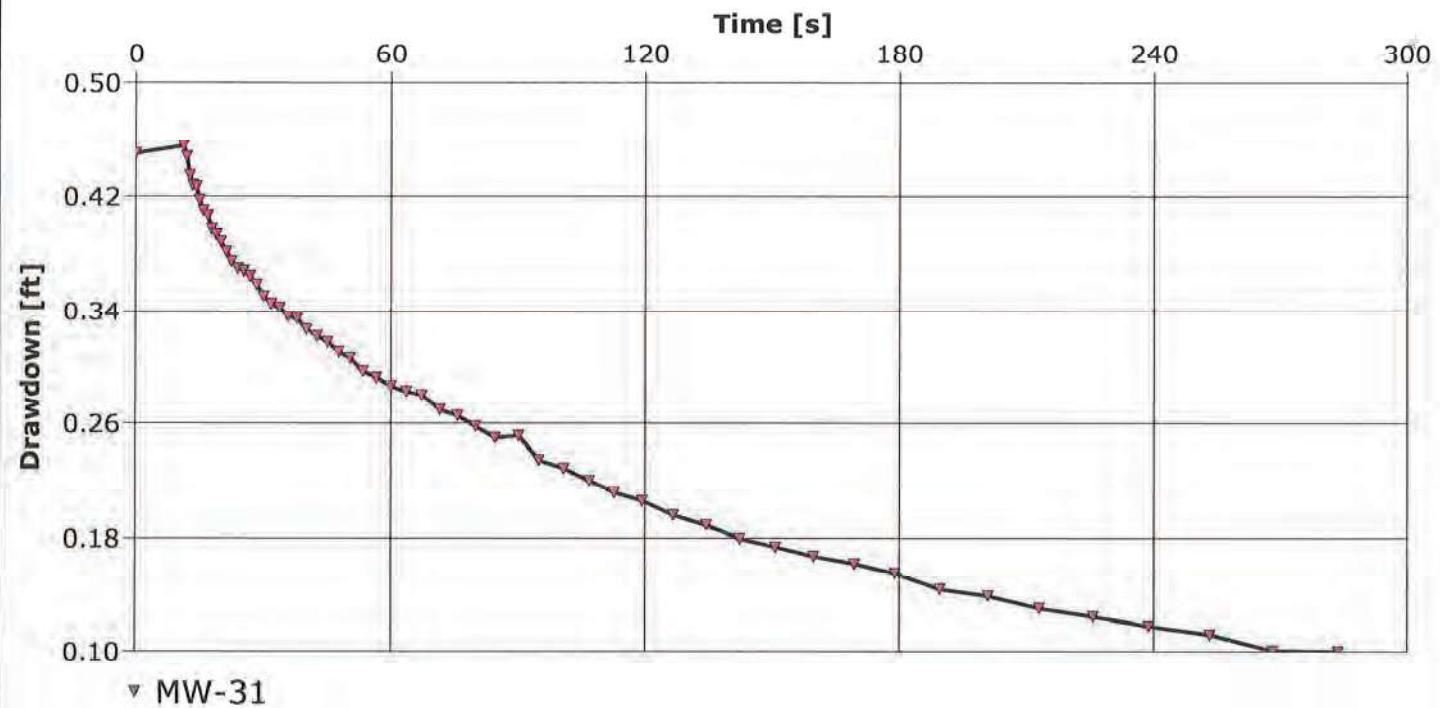
Test Date: 1/28/2016

Analysis Performed by:

MW-31 Slug In Time-Drawdown

Analysis Date: 1/29/2016

Aquifer Thickness: 8.70 ft





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Slug Test Analysis Report

Project: Adams County Landfill

Number: 10-1070.12

Client: Adams County Solid Waste Department

Location: Adams, WI

Slug Test: MW-31 Slug In

Test Well: MW-31

Test Conducted by: Jeff Steiner

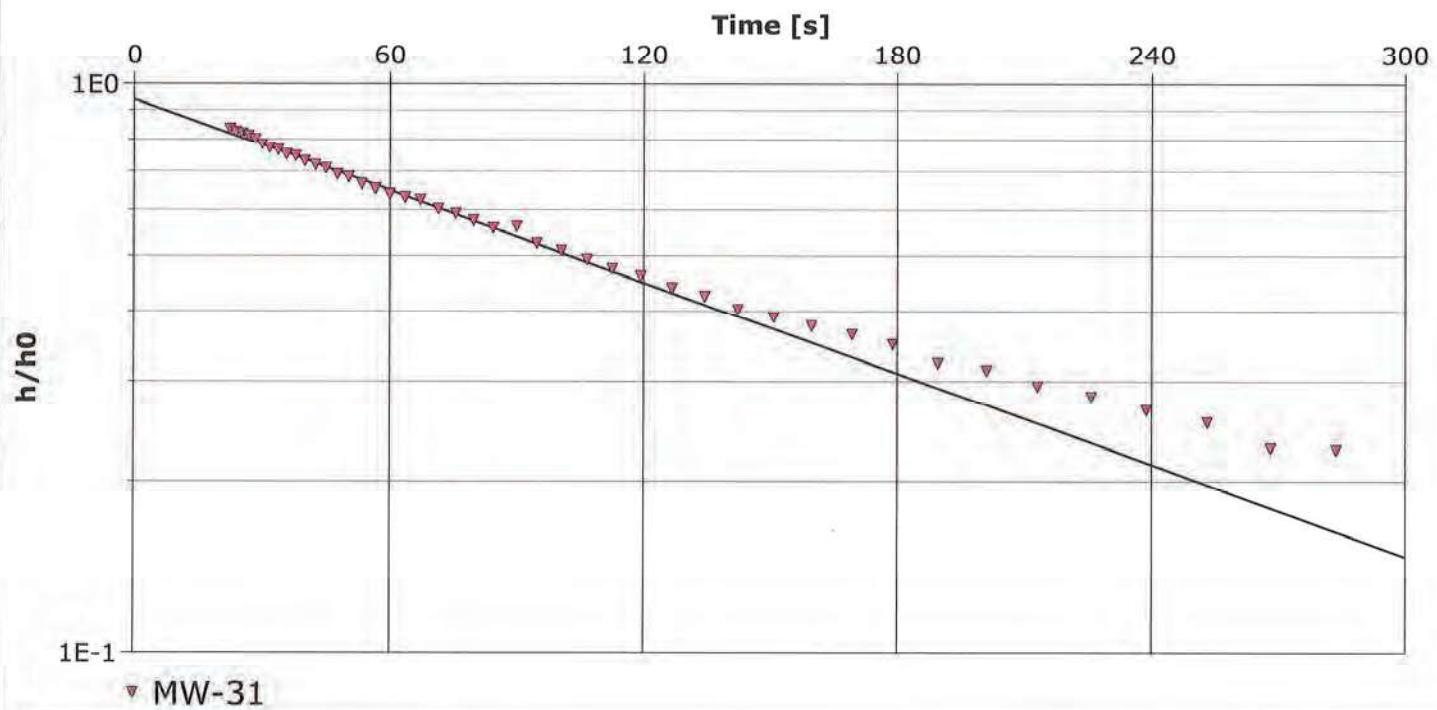
Test Date: 1/28/2016

Analysis Performed by: Jeff Steiner

MW-31 Slug In Bouwer & Rice

Analysis Date: 1/29/2016

Aquifer Thickness: 8.70 ft



Calculation using Bouwer & Rice

| Observation Well | Hydraulic Conductivity [ft/s] | |
|------------------|----------------------------------|--|
| MW-31 | 7.11×10^{-6} | |



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Slug Test Analysis Report

Project: Adams County Landfill

Number: 10-1070.12

Client: Adams County Solid Waste Department

Location: Adams, WI

Slug Test: MW-31 Slug Out

Test Well: MW-31

Test Conducted by: Jeff Steiner

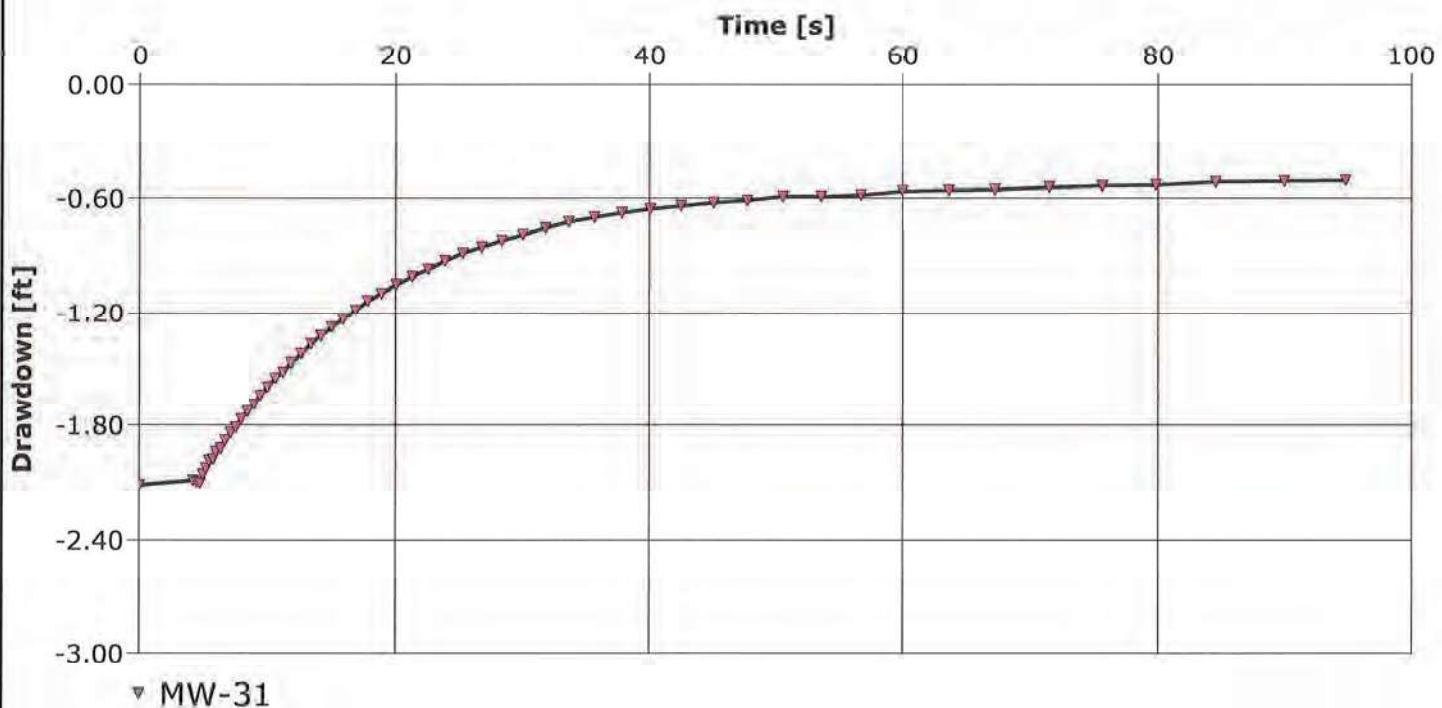
Test Date: 1/28/2016

Analysis Performed by: Jeff Steiner

MW-31 Slug Out Time-Drawdown

Analysis Date: 1/29/2016

Aquifer Thickness: 8.70 ft





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Slug Test Analysis Report

Project: Adams County Landfill

Number: 10-1070.12

Client: Adams County Solid Waste Department

Location: Adams, WI

Slug Test: MW-31 Slug Out

Test Well: MW-31

Test Conducted by: Jeff Steiner

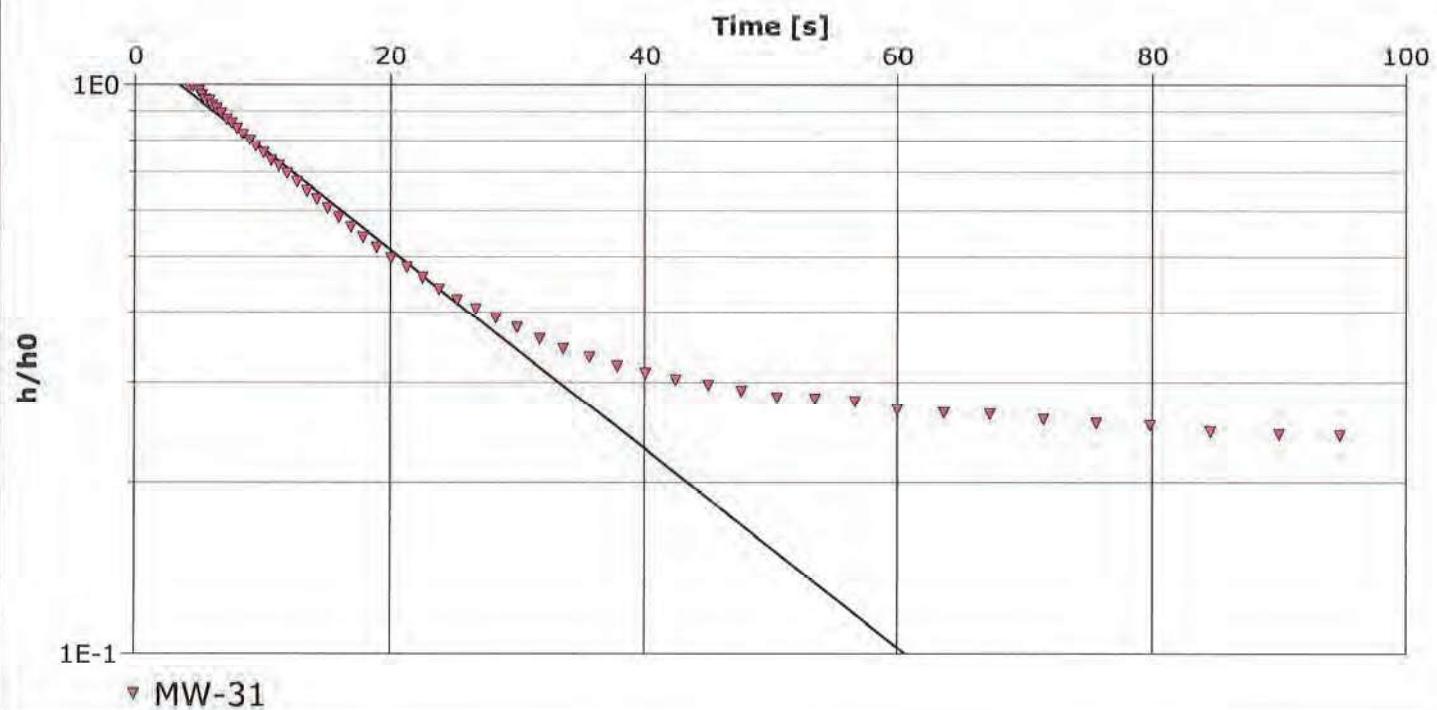
Test Date: 1/28/2016

Analysis Performed by: Jeff Steiner

MW-31 Slug Out Bouwer & Rice

Analysis Date: 1/29/2016

Aquifer Thickness: 8.70 ft



Calculation using Bouwer & Rice

| Observation Well | Hydraulic Conductivity [ft/s] | |
|------------------|----------------------------------|--|
| MW-31 | 4.65×10^{-5} | |

INFIELD PERMEABILITY REPORT

Bail Down Test Methodology

Each bail down test was conducted by initially putting a pressure transducer, with LCD readout in feet, into a well below the static water level. After recording the initial water level, a four foot by 3/4-inch galvanized iron pipe was lowered below the water level, the water was allowed to stabilize and the stabilized reading was recorded. The pipe was then removed from the well. At the instant the minimum water level reading was recorded (a few seconds into the test) a stopwatch was started and rising water level measurements (h) with time (t) were recorded.

The analytical methodology used to evaluate these data is based upon theory presented by Spangler and Handy*.

The formula for hydraulic conductivity is:

$$K = 0.617 * \frac{r * \frac{dh}{dt}}{s * d} * 30.48 \text{ cm/ft}$$

Where:

K = hydraulic conductivity (cm/second)

r = borehole radius (ft)

s = a coefficient which is dependent on the ratios h/d and r/d (Fig. 11-11 of Soil Engineering),

d = depth of borehole below water table (ft).

h = depth (ft) of water in hole at the time dh/dt is determined

dh/dt = rate of rise of water level (ft/second) in hole at depth h, and

t = time (seconds),

* Spangler, M.G. and R.L. Handy, Soil Engineering, 3rd Edition, Intext Educational Publishers, New York, 1973, p. 253-256.

Slug Test Methodology

Each slug test was conducted by initially putting a pressure transducer, with LCD readout in feet, into a well below the static water level. After recording the initial starting level (H), a four foot by 3/4-inch galvanized iron pipe (slug) was lowered below the water level and the maximum water level reading (H_0) recorded. At the instant this maximum water level was reached (a few seconds into the test), a stopwatch was started and declining water level measurements (h) with time (t) were recorded.

Also noted for the purposes of data evaluation were the well casing diameter (r), the boring diameter (R), and the well screen length (L).

The analytical methodology used to evaluate these data is based upon theory presented by Freeze and Cherry*. The formula for hydraulic conductivity (K) is:

$$K = \frac{r^2 \ln(L/R)}{2 LT_0}$$

The key variable in this equation is T_0 , the basic time lag. T_0 is derived by plotting the natural logarithm of the residual head ratio (RHR - the ratio of $[h-H]$, the difference between the maximum rise in water level and the starting water level), against the time (t) at which the head measurement (h) was taken. On semi-log paper these points plot as a straight line.

FIGURE NO. H-1

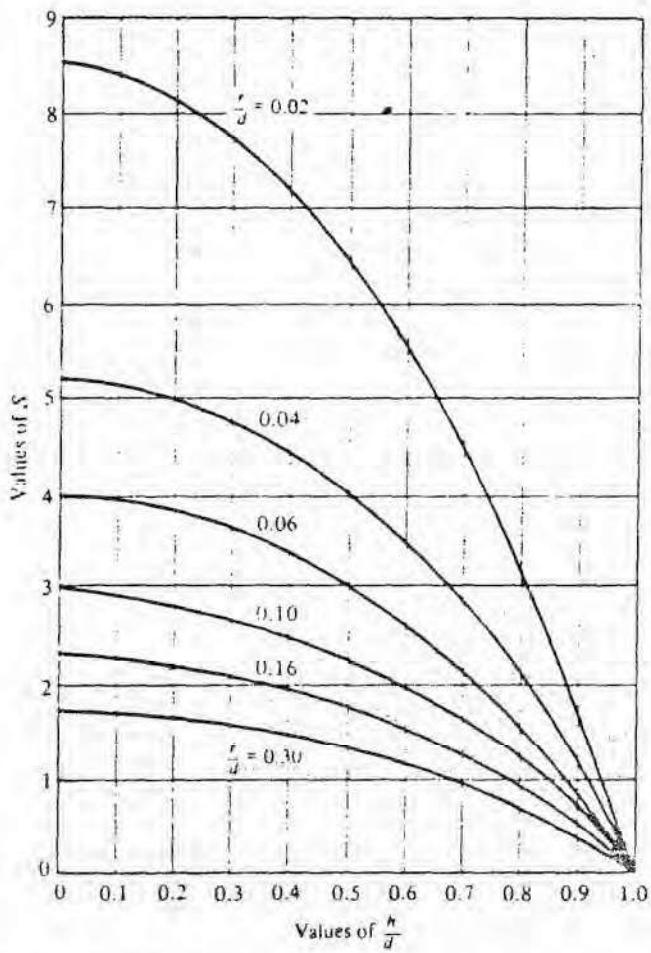


Fig. 11-11. Values of S in Eq. (11-17).

Source: Spangler, M.G. and R.L. Handy, Soil Engineering, 3rd. Edition, Intext Educational Publishers, New York, 1973, p. 255

WATER TABLE MONITORING WELL
HYDRAULIC CONDUCTIVITY SUMMARY

| <u>Well</u> | <u>t</u> (sec) | <u>r</u> (ft) | <u>d</u> (ft) | <u>r/d</u> | <u>h</u> (ft) | <u>h/d</u> | <u>s</u> | <u>dh/dt</u> (ft/s) | <u>K</u> (cm/s) |
|-------------|-------------------|------------------|------------------|------------|------------------|------------|----------|------------------------|----------------------|
| MW-1* | 10 | 0.292 | 11.95 | 0.02 | 11.89 | 0.99 | 0.1 | 0.015 | 6.9×10^{-2} |
| MW-2* | 40 | 0.292 | 12.56 | 0.02 | 11.90 | 0.95 | 0.8 | 0.002 | 1.1×10^{-3} |
| MW-3* | 15 | 0.292 | 13.32 | 0.02 | 12.62 | 0.95 | 0.8 | 0.015 | 7.7×10^{-3} |
| MW-6 | 15 | 0.333 | 11.60 | 0.03 | 10.90 | 0.94 | 0.8 | 0.007 | 4.7×10^{-3} |
| MW-7 | 5 | 0.333 | 5.62 | 0.06 | 5.24 | 0.93 | 0.6 | 0.022 | 4.1×10^{-2} |
| MW-8 | 15 | 0.333 | 7.21 | 0.05 | 6.71 | 0.93 | 0.7 | 0.007 | 8.7×10^{-3} |
| MW-9 | 10 | 0.333 | 3.53 | 0.09 | 3.02 | 0.86 | 1.0 | 0.0075 | 1.3×10^{-2} |
| MW-16 | 15 | 0.333 | 6.70 | 0.05 | 6.18 | 0.92 | 0.8 | 0.014 | 1.6×10^{-2} |
| MW-17 | 15 | 0.333 | 10.58 | 0.03 | 9.84 | 0.93 | 1.1 | 0.010 | 5.4×10^{-3} |
| MW-18 | 15 | 0.333 | 6.40 | 0.05 | 5.91 | 0.92 | 0.8 | 0.013 | 1.6×10^{-2} |

*Screen wrapped in filter fabric

The slope of this line is used to determine the time (t) at which $\ln(RHR)$ is -1. This time value is T_o , which is then used in the above equation to calculate the value of hydraulic conductivity for the test.

* Freeze, R.A. and J.A. Cherry, Groundwater,
Prentice-Hall, Inc. Englewood Cliffs, New Jersey,
1979, pp. 340-341.

IN FIELD HYDRAULIC CONDUCTIVITY SUMMARY
PIEZOMETER RESULTS - SLUG TEST METHOD

| <u>Well</u> | <u>K (cm/s)</u> |
|-------------|----------------------|
| MW-3P | 2.4×10^{-4} |
| MW-6P | 4.5×10^{-4} |
| MW-7P | 2.2×10^{-3} |
| MW-18P | 4.6×10^{-4} |

ADAMS COUNTY LANDFILL
FEASIBILITY STUDY PERMEABILITY TESTS
SLUG TEST RESULTS: WELL 3P

$$\text{Equation: } K = \frac{r^2 \ln(L/R)}{2 L T_o}$$

r = well radius = 2.54 cm

L = screen sand pack length = 228.60 cm

R = borehole radius = 5.08 cm

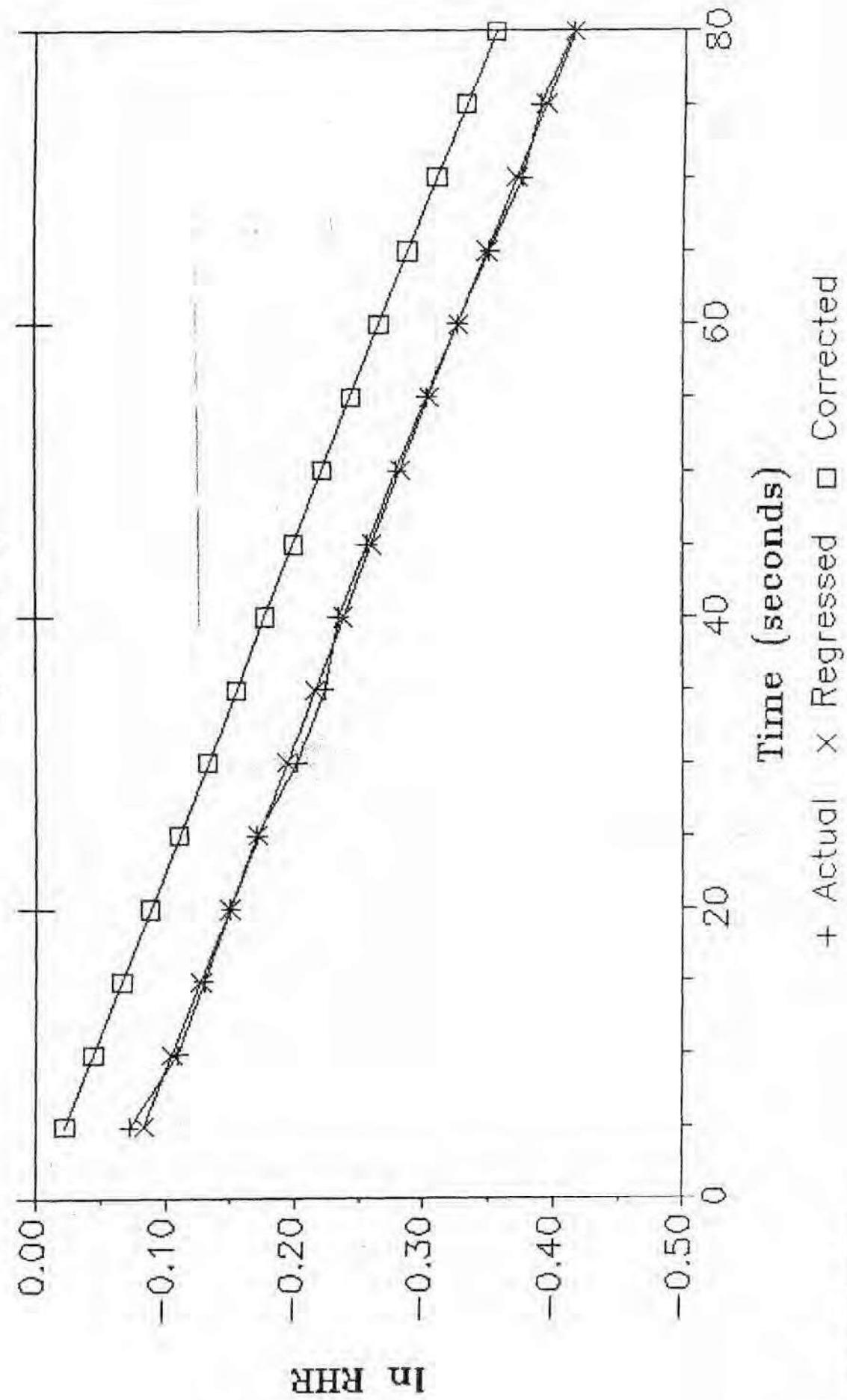
H_o = initial head difference = 1.15 feet

T_o = time lag = 224.8 seconds

---> K = hydraulic conductivity = 2.4×10^{-4} cm/second

Note: - T_o corresponds to the time when the natural log (ln) of the residual head ratio is -1.00
-RHR is the Residual Head Ratio which is the ratio of the unrecovered head difference (H) and the initial head difference (H_o) created by the added/removed water

ADAMS COUNTY LANDFILL
Feasibility Study Permeability Tests
Well MW-3P



ADAMS COUNTY LANDFILL
FEASIBILITY STUDY PERMEABILITY TESTS
SLUG TEST RESULTS: WELL 6P

$$\text{Equation: } K = \frac{r^2 \ln(L/R)}{2 L T_o}$$

r = well radius = 2.54 cm

L = screen sand pack length = 243.84 cm

R = borehole radius = 5.08 cm

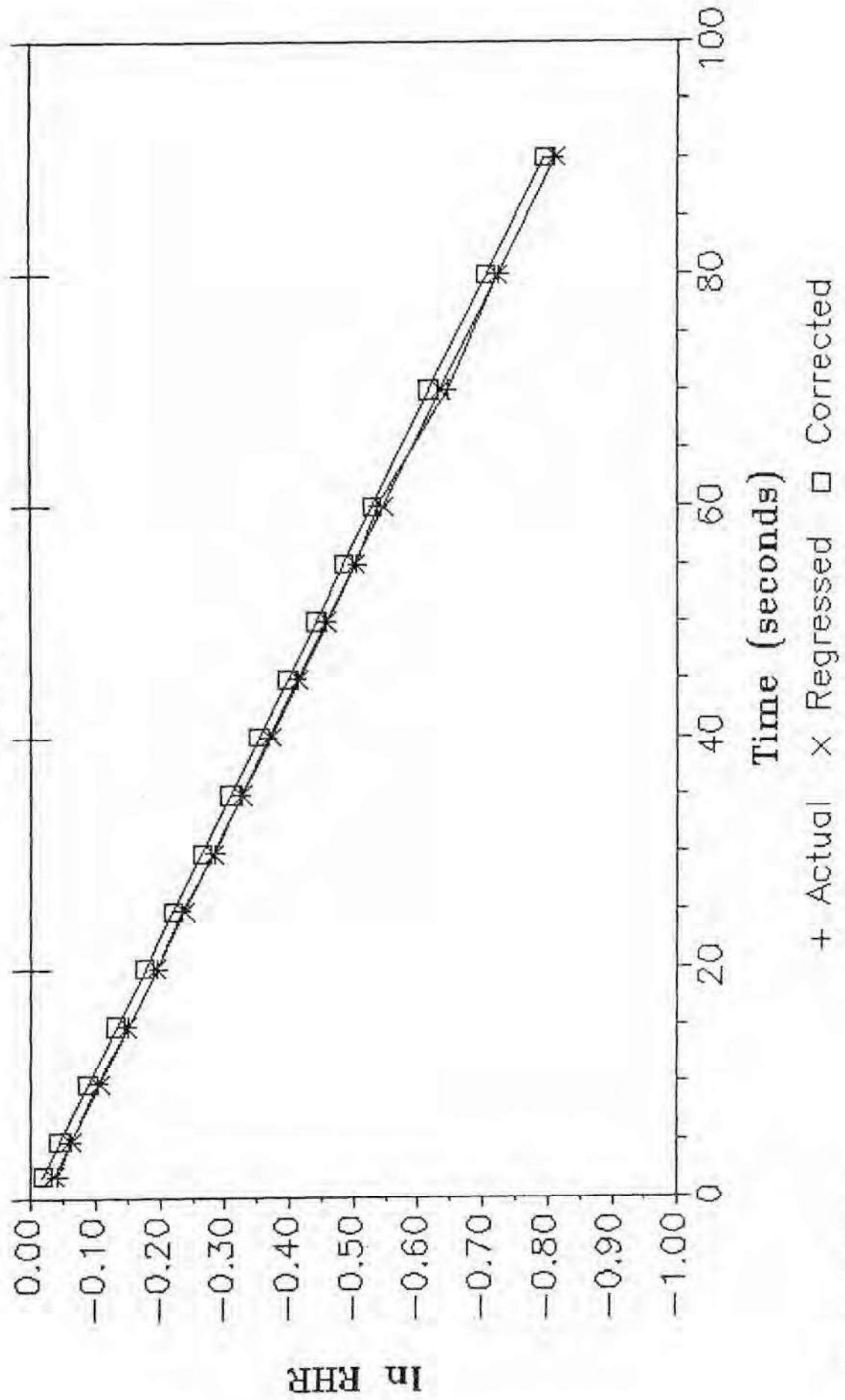
H_o = initial head difference = 1.01 feet

T_o = time lag = 112.9 seconds

---> K = hydraulic conductivity = 4.5×10^{-4} cm/second

Note: -T_o corresponds to the time when the natural log (ln) of the residual head ratio is -1.00
-RHR is the Residual Head Ratio which is the ratio of the unrecovered head difference (H) and the initial head difference (H_o) created by the added/removed water

ADAMS COUNTY LANDFILL
Feasibility Study Permeability Tests
Well MW - 6P



ADAMS COUNTY LANDFILL
FEASIBILITY STUDY PERMEABILITY TESTS
SLUG TEST RESULTS: WELL 7P

$$\text{Equation: } K = \frac{r^2 \ln(L/R)}{2 L T_o}$$

r = well radius = 2.54 cm

L = screen sand pack length = 243.84 cm

R = borehole radius = 5.08 cm

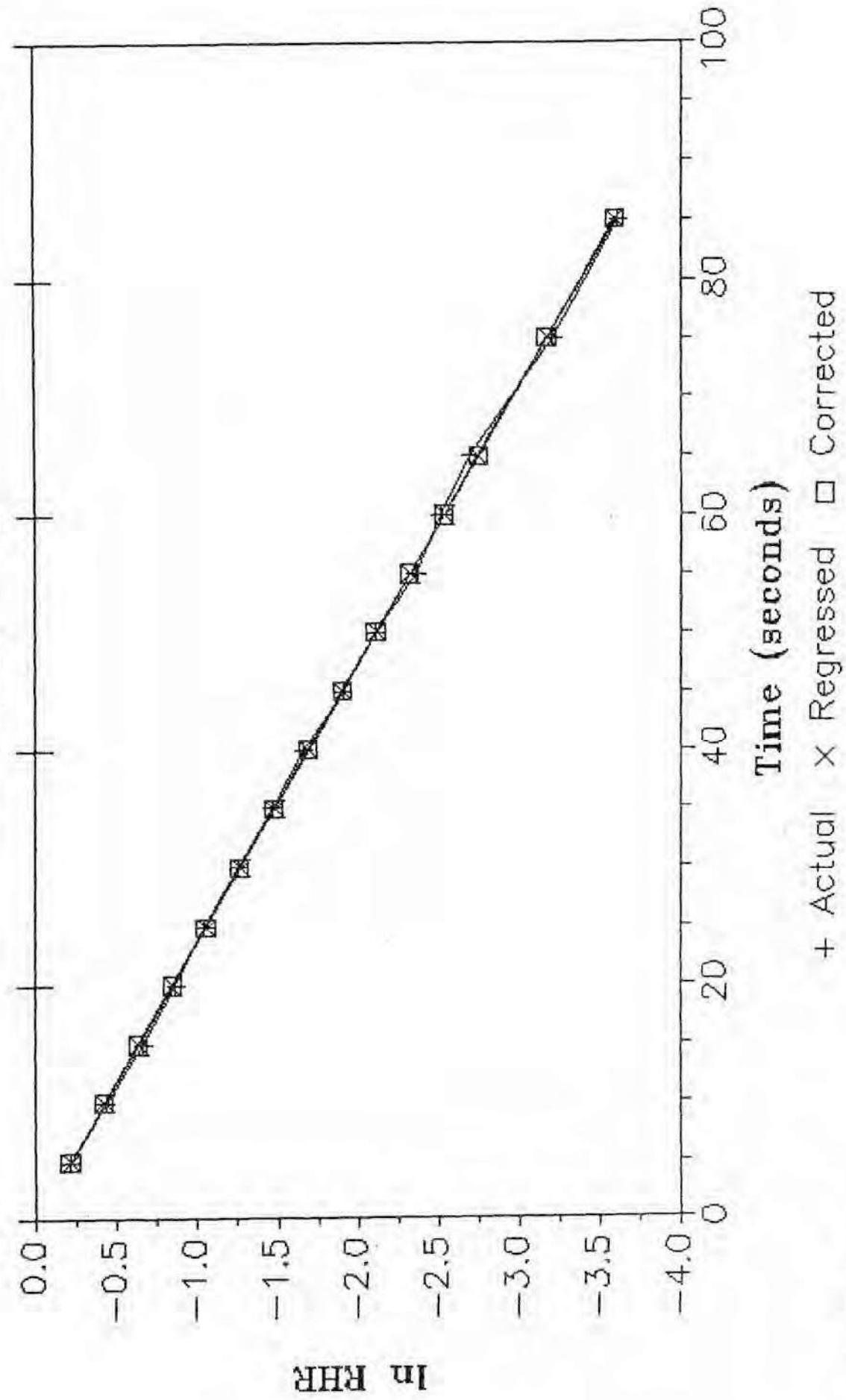
H_o = initial head difference = 0.74 feet

T_o = time lag = 23.6 seconds

---> K = hydraulic conductivity = 2.2×10^{-3} cm/second

Note: - T_o corresponds to the time when the natural log
(ln) of the residual head ratio is -1.00
-RHR is the Residual Head Ratio which is the ratio
of the unrecovered head difference (H) and the
initial head difference (H_o) created by the
added/removed water

ADAMS COUNTY LANDFILL
Feasibility Study Permeability Tests
Well MW - 7P



ADAMS COUNTY LANDFILL
FEASIBILITY STUDY PERMEABILITY TESTS
SLUG TEST RESULTS: WELL 18P

$$\text{Equation: } K = \frac{r^2 \ln(L/R)}{2 L T_o}$$

r = well radius = 2.54 cm

L = screen sand pack length = 228.60 cm

R = borehole radius = 5.08 cm

H_o = initial head difference = 1.39 feet

T_o = time lag = 116.6 seconds

---> K = hydraulic conductivity = 4.6×10^{-4} cm/second

Note: - T_o corresponds to the time when the natural log
(ln) of the residual head ratio is -1.00
-RHR is the Residual Head Ratio which is the ratio
of the unrecovered head difference (H) and the
initial head difference (H_o) created by the
added/removed water

ADAMS COUNTY LANDFILL
Feasibility Study Permeability Tests
Well MW-18P

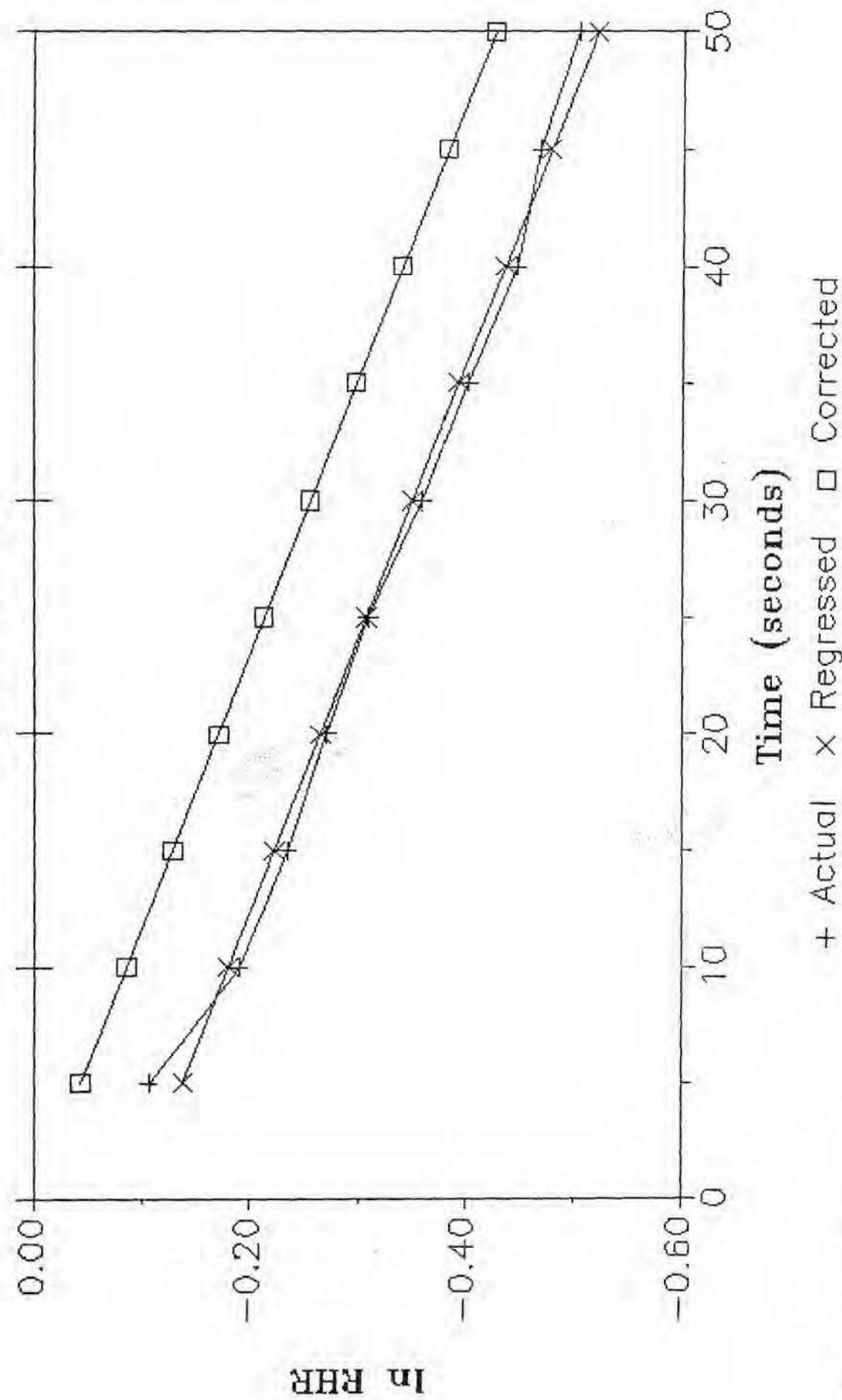


TABLE NO. 6-7

IN-FIELD PERMEABILITY TESTS

| Well | Hydraulic Conductivity (cm/sec) | Soil Type | Well Screen Elevation (USGS) |
|--------|------------------------------------|-------------|---------------------------------|
| MW-1 | 6.9×10^{-2} | SP;CL | 935 - 920 |
| MW-2 | 1.1×10^{-3} | SP;CL | 943 - 928 |
| MW-3 | 7.7×10^{-3} | SP;CL | 938 - 923 |
| MW-3P | 2.4×10^{-4} | SP | 897 - 892 |
| MW-6 | 4.7×10^{-3} | SP;CL,ML | 945 - 930 |
| MW-6P | 4.5×10^{-4} | SP | 907 - 902 |
| MW-7 | 4.1×10^{-2} | SM | 943 - 933 |
| MW-7P | 2.2×10^{-3} | SP | 909 - 904 |
| MW-8 | 8.7×10^{-3} | SM;SP,CL | 943 - 933 |
| MW-9 | 1.3×10^{-2} | SM;SP | 942 - 932 |
| MW-16 | 1.6×10^{-2} | ML,CL,SM | 945 - 935 |
| MW-17 | 5.4×10^{-3} | ML,CL,SM | 943 - 933 |
| MW-18 | 1.6×10^{-2} | SP;ML,CL,SM | 944 - 934 |
| MW-18P | 4.6×10^{-4} | SP | 908 - 903 |

Foth & Van Dyke

Engineers/Architects

2737 S. Ridge Road
P. O. Box 19012
Green Bay, Wisconsin 54307-9012
414/497-2500

FALLING/CONSTANT HEAD TEST

| | |
|--|--|
| No. of Layers | |
| No. of Blows/Hammer Size | |
| Vol. of Water Added (c.c.) | |
| Wt. of Cyl. + Soil, Wm (lbs.) | |
| Wt. of Cyl., Wc (lbs.) | |
| Wt. of Soil, W (lbs.) | |
| Average Water Content, w(%) | |
| Moist Density, FM (lbs./ft. ³) | |
| Dry Density, FM (dry) (lbs./ft. ³) | |
| % Compaction | |

| | |
|--|---------------|
| JOB NO.: | 86A22 |
| BORING NO.: | 10 |
| SAMPLE NO.: | FR-17 |
| DEPTH: | 30-33' |
| TUBE DIAMETER | A = 2.80" |
| LENGTH OF SAMPLE | 6.8125" |
| DIST. FROM TOP OF TUBE TO LOWER WATER LEVEL | 26.3 cm |
| DATE: | July 18, 1986 |
| TECH. NAME: | R. Rouse |

| | TIME AM/PM | DATE | TIME INTERVAL (MIN.) | H @ START OF TEST | H @ FINISH | TARE | TOTAL WT. TARE + WATER, GR. | WEIGHT OF WATER, GR. | K CM/SEC. |
|------|-------------------------|--------------------------------|----------------------------|-------------------------|---------------|-----------|--------------------------------------|-------------------------------|-----------------------|
| (1) | 08:05 16:08 | AM/PM 7/18/86 AM/PM 7/18/86 | (483) 28,980 | SATURATION 101.0 | 96.1 | 201.7 | 299.8 | 98.1 | 2.50×10^{-6} |
| (2) | 16:08 10:37 | AM/PM 7/18/86 AM/PM 7/21/86 | (3985) 239,100 | -- 96.1 | 83.3 | 201.7 | 436.7+ | 235.0+ | 9.00×10^{-7} |
| (3) | 10:37 07:32 | AM/PM 7/21/86 AM/PM 7/22/86 | (1255) 75,300 | @ 2 psi 83.3 | 74.6 | 201.7 | 379.8 | 178.1 | 8.00×10^{-7} |
| (4) | 07:32 07:11 | AM/PM 7/22/86 AM/PM 7/23/86 | (1419) 85,140 | -- 74.6 | 72.2 | 201.7 | 246.4 | 44.7 | 5.00×10^{-7} |
| (5) | 07:11 22:58 | AM/PM 7/23/86 AM/PM 7/26/86 | (5267) 316,020 | -- 72.2 | 66.3 | 201.7 | 312.6 | 110.9 | 4.00×10^{-7} |
| (6) | 22:58 09:43 | AM/PM 7/26/86 AM/PM 7/29/86 | (3525) 211,500 | -- 66.3 | 62.9 | 201.7 | 260.7 | 59.0 | 4.00×10^{-7} |
| (7) | 09:43 14:33 | AM/PM 7/29/86 AM/PM 8/04/86 | (8930) 535,800 | @ 2 psi 62.9 | 55.7 | 201.7 | 330.1 | 128.4 | 9.61×10^{-8} |
| (8) | 14:33 11:43 | AM/PM 8/04/86 AM/PM 8/10/86 | (8470) 508,200 | @ 1 psi 55.7 | 49.4 | 201.7 | 310.0 | 108.3 | 1.00×10^{-7} |
| (9) | 11:43 07:38 | AM/PM 8/10/86 AM/PM 8/12/86 | (2635) 158,100 | @ 1 psi 49.4 | 47.7 | 201.7 | 231.0 | 29.3 | 1.00×10^{-7} |
| (10) | 07:38 13:10 | AM/PM 8/12/86 AM/PM 8/18/86 | (8972) 538,320 | @ 1 psi 47.7 | 41.2 | 201.7 | 318.7 | 117.0 | 2.00×10^{-7} |
| (11) | 13:10 09:20 | AM/PM 8/18/86 AM/PM 8/21/86 | (4090) 245,400 | @ 1 psi 41.2 | 38.2 | 201.7 | 251.9 | 50.2 | 2.00×10^{-7} |
| (12) | 09:20 AM/PM AM/PM | AM/PM 8/21/86 AM/PM 8/25/86 | (5760) 345,600 | @ 1 psi 38.2 | 34.3 | 201.7 | -- | -- | 2.00×10^{-7} |
| | AM/PM AM/PM | | | | | Perm Rate | | | 2×10^{-7} |

Foth & Van Dyke

Engineers/Architects

2737 S. Ridge Road
P. O. Box 19012
Green Bay, Wisconsin 54307-9012
414/497-2500

PROJECT: Adams County Feasibilit

JOB NO.: 86A22

DATE: September 11, 1986

PERMEABILITY TEST CONSTANT HEAD

SAMPLE NO.: FR-25 - Boring #11 at 10' to 15' depth

SOIL DESCRIPTION: SAND, fine to medium grained, light brown (SP)

% COMPACTION --

COMPACTED DRY DENSITY = 103.3pcf

MOISTURE = 7.4%

SAMPLE DIAMETER = 4.00"

SAMPLE HEIGHT = 4.5625" (4-9/16")

| RUN NO. | HEAD, MM ² | DURATION, MM ² | PERMEABILITY, CM/SEC. | REMARKS |
|------------------|-----------------------|---------------------------|-----------------------|---------|
| 1 | 83.0 | 15 | 1.06×10^{-2} | |
| 2 | 83.0 | 15 | 1.03×10^{-2} | |
| 3 | 83.0 | 15 | 1.03×10^{-2} | |
| 4 | 83.0 | 15 | 1.05×10^{-2} | |
| 5 | 83.0 | 15 | 1.04×10^{-2} | |
| Average for Test | | | 1.04×10^{-2} | |
| Perm Rate | | | 1×10^{-2} | |

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PROJECT: Adams County Feasibil

JOB NO.: 86A22

DATE: September 11, 1986

PERMEABILITY TEST CONSTANT HEAD

SAMPLE NO.: FR-21 - Boring #12 at 5' to 10' depth

SOIL DESCRIPTION: SILTY SAND, fine grained, light brown (SM)

% COMPACTION 92

COMPACTED DRY DENSITY = 106.7pcf

MOISTURE = 10.4%

SAMPLE DIAMETER = 4.0"

SAMPLE HEIGHT = 4.5625"

| RUN NO. | HEAD, INCHES | (CM) | DURATION, MINUTES | (Seconds) | PERMEABILITY, CM/SEC. | REMARKS |
|------------------|--------------|------|-------------------|-----------|-----------------------|---------|
| 1 | 84.5 | | | 30 | 6.60×10^{-4} | |
| 2 | 84.5 | | | 30 | 6.43×10^{-4} | |
| 3 | 84.5 | | | 30 | 6.77×10^{-4} | |
| 4 | 84.5 | | | 30 | 6.77×10^{-4} | |
| 5 | 84.5 | | | 30 | 6.43×10^{-4} | |
| Average of Tests | | | | | 6.60×10^{-4} | |
| Perm Rate | | | | | 7×10^{-4} | |

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2727 S. Ridge Road

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P. O. Box 12212

P. O. Box 19012

Green Bay, Wisconsin 54307-9012

414/497-2500

FALLING/CONSTANT HEAD TEST

| | |
|--|--|
| No. of Layers | |
| No. of Blows/Hammer Size | |
| Vol. of Water Added (c.c.) | |
| Wt. of Cyl. + Soil, Wm (lbs.) | |
| Wt. of Cyl., Wc (lbs.) | |
| Wt. of Soil, W (lbs.) | |
| Average Water Content, w(%) | |
| Moist Density, FM (lbs./ft. ³) | |
| Dry Density, FM (dry) (lbs./ft. ³) | |
| % Compaction | |

| | |
|--|---------------|
| JOB NO.: | 86A22 |
| BORING NO.: | 12 |
| SAMPLE NO.: | FR-16 |
| DEPTH: | 32' |
| TUBE DIAMETER | A = 2.80" |
| LENGTH OF SAMPLE | 7.0" |
| DIST. FROM TOP OF TUBE TO LOWER WATER LEVEL | 26.0 cm |
| DATE: | July 16, 1986 |
| TECH. NAME: | R. Rouse |

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Green Bay, Wisconsin 54307-9012
414/497-2500

PROJECT: Adams County Study

JOB NO.: 86A22

DATE: September 10, 1986

PERMEABILITY TEST CONSTANT HEAD

SAMPLE NO.: FR-20

Boring #13 at 10' - 13' depth

SOIL DESCRIPTION: Sand, fine grained, brown (SP)

% COMPACTION = 91 1/2

COMPACTED DRY DENSITY = 101.7 pcf

MOISTURE = 5.6%

SAMPLE DIAMETER = 4.00"

SAMPLE HEIGHT = 4.5625" (4 9/16")

| RUN NO. | HEAD, CM | DURATION, SECONDS | PERMEABILITY, CM/SEC. | REMARKS |
|--|----------|-------------------|-----------------------|---------|
| 1 | 82.1 | 15 | 7.66×10^{-3} | |
| 2 | 82.1 | 15 | 7.37×10^{-3} | |
| 3 | 82.1 | 15 | 7.40×10^{-3} | |
| 4 | 82.1 | 15 | 7.31×10^{-3} | |
| 5 | 82.1 | 15 | 7.09×10^{-3} | |
| Average of Tests = 7.37×10^{-3} | | | | |

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Green Bay, Wisconsin 54307-9012

Green Bay, WI
414/497-2500

FALLING/CONSTANT HEAD TEST

Recompacted Perm

| | |
|--|--------|
| No. of Layers | 4 |
| No. of Blows/Hammer Size | 25/10# |
| Vol. of Water Added (c.c.) | |
| Wt. of Cyl. + Soil, Wm (lbs.) | 5409 |
| Wt. of Cyl., Wc (lbs.) | 3357 |
| Wt. of Soil, W (lbs.) | 2052 |
| Average Water Content, w(%) | 11.1 |
| Moist Density, FM (lbs./ft. ³) | 135.7 |
| Dry Density, FM (dry) (lbs./ft. ³) | 122.2 |
| % Compaction | 95 |

| | |
|--|-----------------------|
| JOB NO.: | 86A22 FR |
| BORING NO.: | MW-8 |
| SAMPLE NO.: | |
| DEPTH: | 50-55' |
| | |
| TUBE DIAMETER | A = 4.0" |
| LENGTH OF SAMPLE | 4.50 |
| DIST. FROM TOP OF TUBE TO LOWER WATER LEVEL | 33.2 cm |
| DATE: | September 13-19, 1986 |
| TECH. NAME: | RRR |

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PROJECT: Adams County Study

JOB NO.: 86A22 FR

DATE: September 10, 1986

PERMEABILITY TEST CONSTANT HEAD

SAMPLE NO.: FR-19

Boring MW-9 at 10' depth

SOIL DESCRIPTION: Sand, fine grained, brown (SP)

% COMPACTION - 90

COMPACTED DRY DENSITY = 100.1 pct

MOISTURE = 1.7%

SAMPLE DIAMETER = 4.00"

SAMPLE HEIGHT = 4.5625 (4 9/16")

| <u>RUN NO.</u> | <u>HEAD, CM.</u> | <u>Seconds</u> | <u>DURATION, MINUTES</u> | <u>PERMEABILITY, CM/SEC.</u> | <u>REMARKS</u> |
|--------------------|------------------|----------------|--------------------------|------------------------------|----------------|
| 1 | 82.7 cm | 15 | | 8.54×10^{-3} | |
| 2 | 82.7 cm | 15 | | 8.49×10^{-3} | |
| 3 | 82.7 cm | 15 | | 8.47×10^{-3} | |
| 4 | 82.7 cm | 15 | | 7.95×10^{-3} | |
| 5 | 82.7 cm | 15 | | 7.88×10^{-3} | |
| Average of Tests = | | | | 8.27×10^{-3} | |